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▶ Thermal Bridging Modeling with Benchmarking

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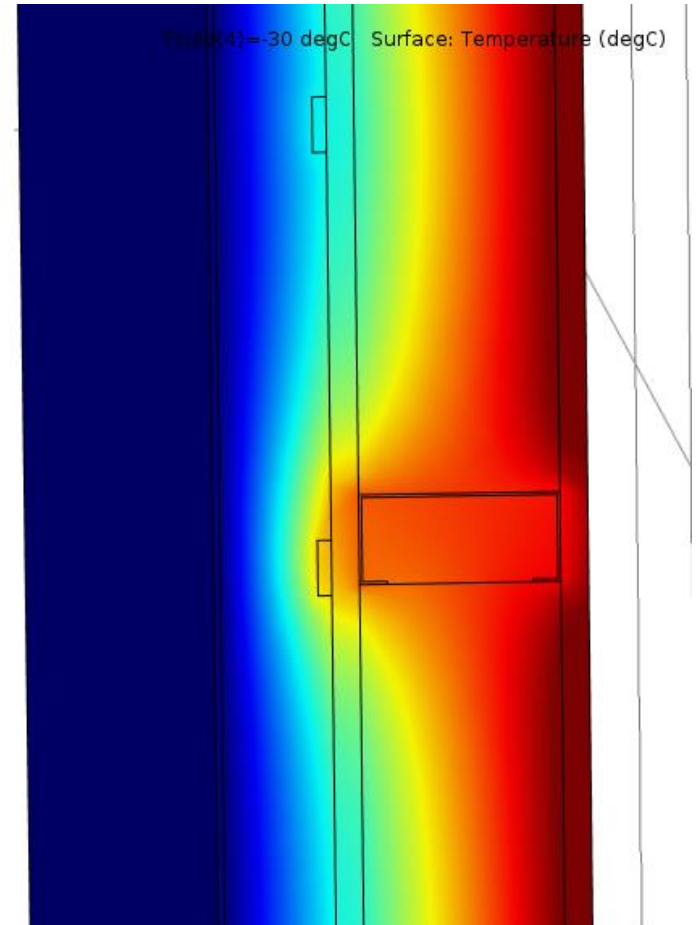


Outline

- Project description
- Wall assemblies
- Experiments
- Numerical simulations
- Results
- Benchmarking
- Conclusion

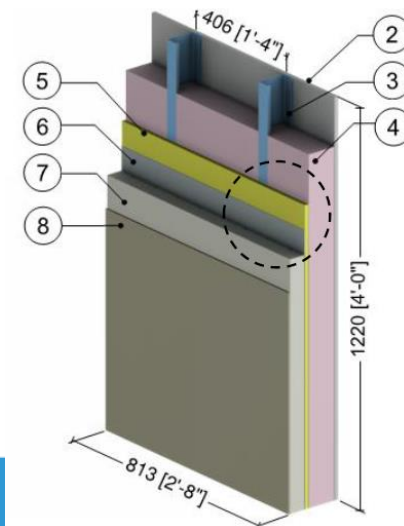
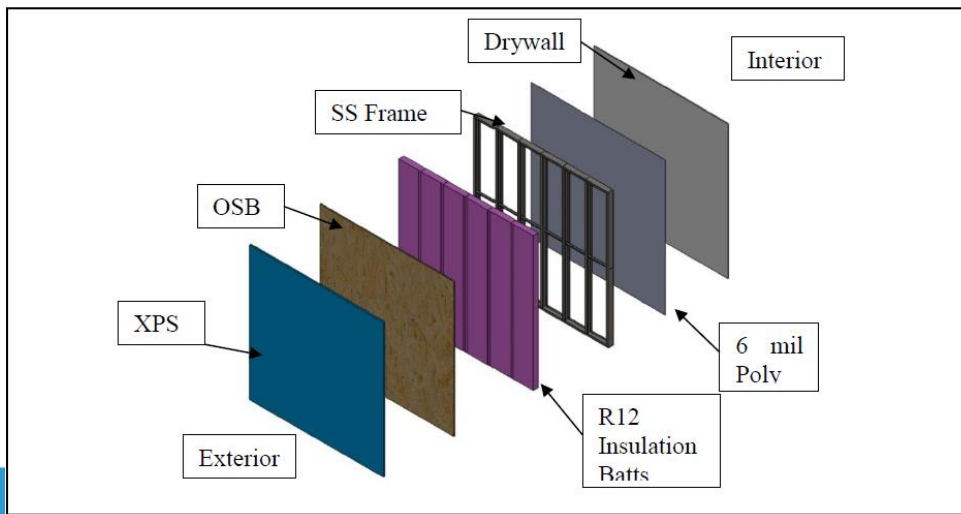
Project Description

- Pan-Canadian climate plan, which is adopted in 2016, requires Canada to meet its 2030 emissions target
- 17% of Canada's GHG emissions are due to buildings
- Thermal bridging can greatly affect the thermal performance of assemblies specially in high performance buildings
- This project includes guarded hot box testing of seven wall assemblies and COMSOL simulation of 27 wall assemblies in one year
- Numerical results for three WAs are benchmarked against Guarded Hot Box (GHB) test results.



Summary of the walls that were tested

| ID | ASHRAE ID | Interior Sheathing | Fiberglass Cavity Insulation | Cavity Depth | Steel Stud Thickness | Steel Stud Spacing (o.c.) | Steel Stud Flange | Steel Track Thickness | Steel Track Flange | Exterior Sheathing | Exterior Insulation | Cladding |
|----|-----------|---------------------------|------------------------------|-------------------|----------------------|---------------------------|-------------------|-----------------------|--------------------|------------------------|---------------------|----------|
| W1 | SS. 19 | 1/2" (13 mm) gypsum | R-12 (RSI 2.1) | 3 5/8" (92 mm) | 20 gauge | 16" (406 mm) | 1 5/8" (41 mm) | 1.03 mm | Not stated | 5/8" (16 mm) OSB | none | none |
| W2 | SS. 20 | 1/2" (13 mm) gypsum | R-12 (RSI 2.1) | 3 5/8" (92 mm) | 20 gauge | 16" (406 mm) | 1 5/8" (41 mm) | 1.03 mm | Not stated | 5/8" (16 mm) OSB | 1" (25mm) XPS | none |
| W3 | SS. 21 | 1/2" (13 mm) gypsum | R-12 (RSI 2.1) | 3 5/8" (92 mm) | 20 gauge | 16" (406 mm) | 1 5/8" (41 mm) | 1.03 mm | Not stated | 5/8" (16 mm) OSB | 2" (50mm) XPS | none |



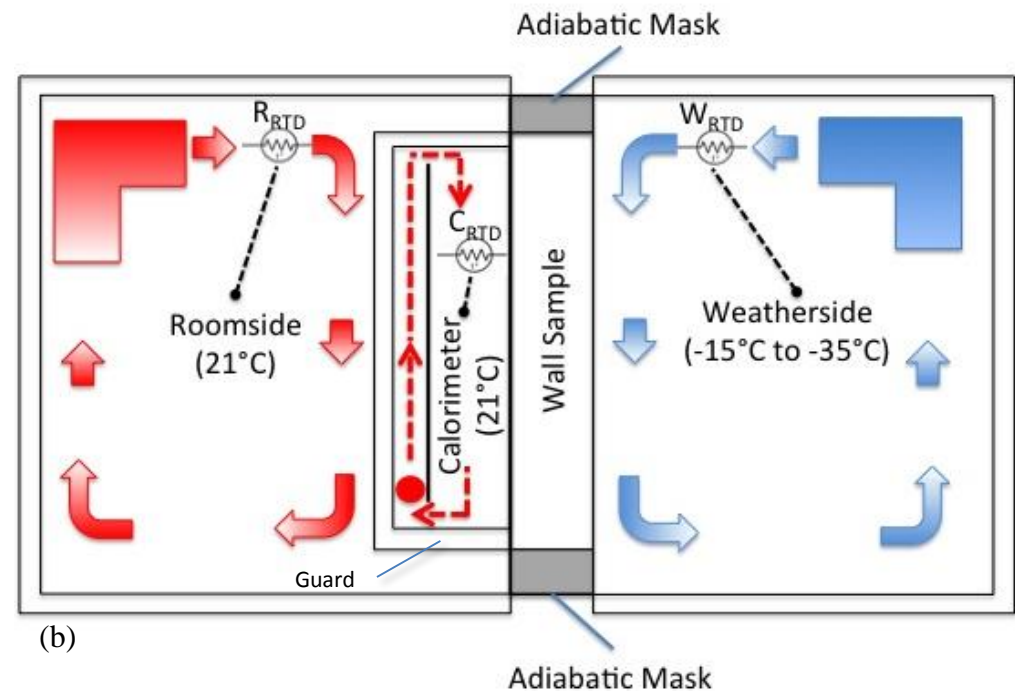
Experiments: Guarded Hot Box (GHB)

$$RSI = \frac{A * \Delta T}{Q}$$

Q = the heat input to the calorimeter (W)

A = the specimen area normal to the direction of heat transfer (m^2)

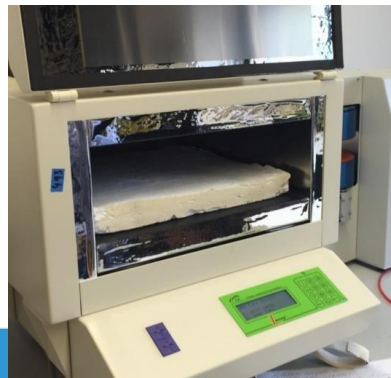
ΔT = the absolute temperature difference between the interior and exterior air ($^{\circ}K$)



Temperature dependent conductivity

- The temperature dependent conductivity of the materials used in the wall assemblies tested in the GHB.

| Material | Thickness (mm) | T_{mean} | RSI ($\text{m}^2\text{K}/\text{W}$) | Fitted Equation for R | K ($\text{W}/(\text{m}\cdot\text{K})$) | Fitted Equation for K |
|-------------|----------------|-------------------|---------------------------------------|----------------------------------|--|-----------------------------------|
| OSB | 6 | 24.68 | 0.123 | $0.13(1-0.0019T_{\text{mean}})$ | 0.0487 | $K=0.0464+0.00009T_{\text{mean}}$ |
| | | 12.95 | 0.126 | | 0.047 | |
| | | 0.58 | 0.129 | | 0.0465 | |
| Glass-fiber | 89 | 24.08 | 2.248 | $2.603(1-0.0057T_{\text{mean}})$ | 0.0395 | $K=0.0342+0.0002T_{\text{mean}}$ |
| | | 11.99 | 2.421 | | 0.0367 | |
| | | -0.6 | 2.606 | | 0.034 | |
| XPS | 25 | 23.95 | 0.88 | $0.97(1-0.0042T_{\text{mean}})$ | 0.0284 | $K=0.0255+0.0001T_{\text{mean}}$ |
| | | 11.93 | 0.928 | | 0.0269 | |
| | | 0 | 0.978 | | 0.0255 | |
| XPS | 50 | 24.02 | 1.73 | $1.939(1-0.0045T_{\text{mean}})$ | 0.0289 | $K=0.0258+0.0001T_{\text{mean}}$ |
| | | 12.04 | 1.832 | | 0.0272 | |
| | | 0.02 | 1.939 | | 0.0257 | |



Temperature dependent conductivity

The screenshot displays the COMSOL Multiphysics software interface for a model named "SS19 NRC.mph". The main window shows a 3D perspective view of a rectangular wall assembly. The left sidebar contains the Model Builder tree, and the center pane shows the Settings for an Analytic function.

Settings - Analytic

Label: Analytic 1
Function name: Kfib1

Definition

Expression: $0.03438 + 0.000212 \cdot (T - 273.15)$
Arguments: T
Derivatives: Automatic

Periodic Extension

Units

Arguments: K
Function: W/(m*K)

Advanced

Plot Parameters

| Argument | Lower limit | Upper limit |
|----------|-------------|-------------|
| T | 230 | 300 |

Messages Progress Log Evaluation 3D

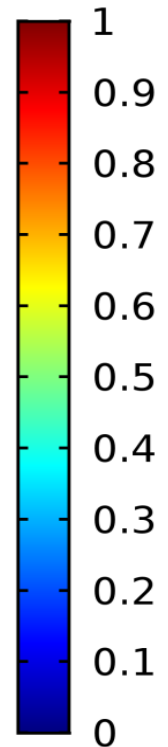
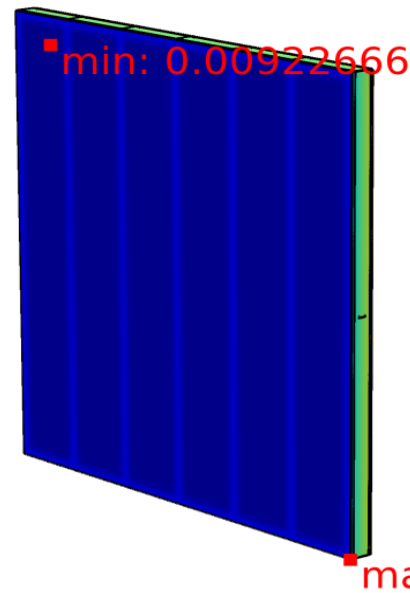
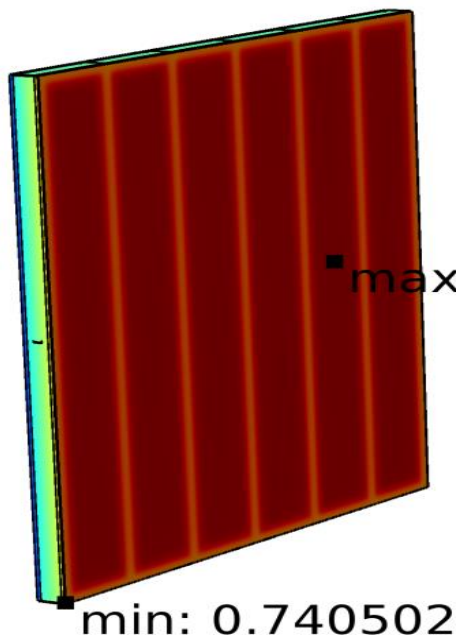
| x | y | z | Value |
|----------|---------|----------|--------|
| -0.36153 | 0.27163 | 0.035283 | 16.771 |

6.78 GB | 6.98 GB

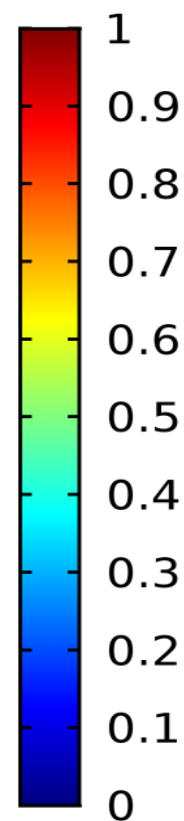
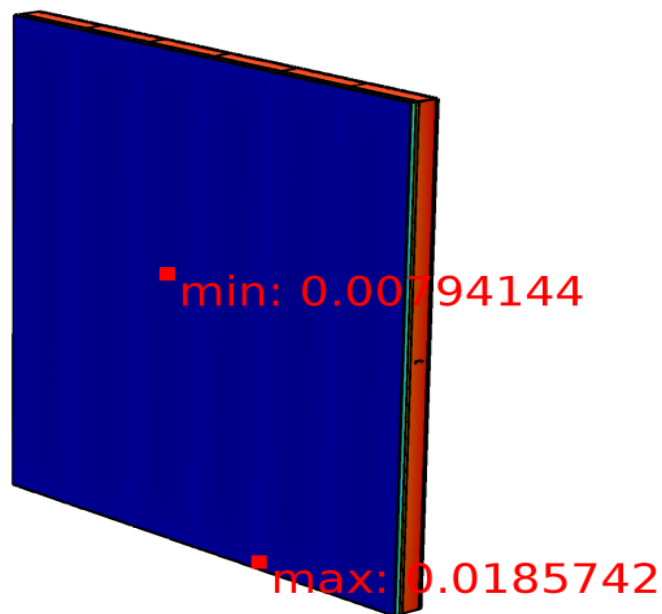
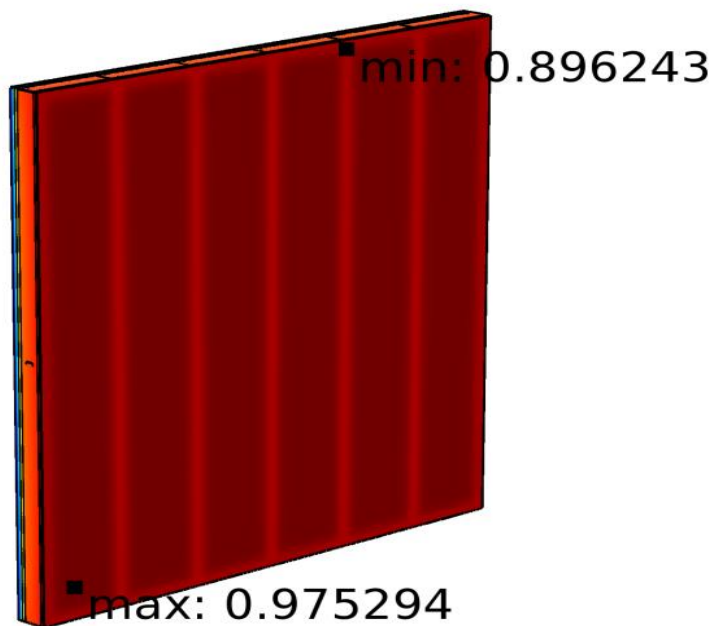
1:44 PM
1/17/2018

W1 Surface Temperature Index

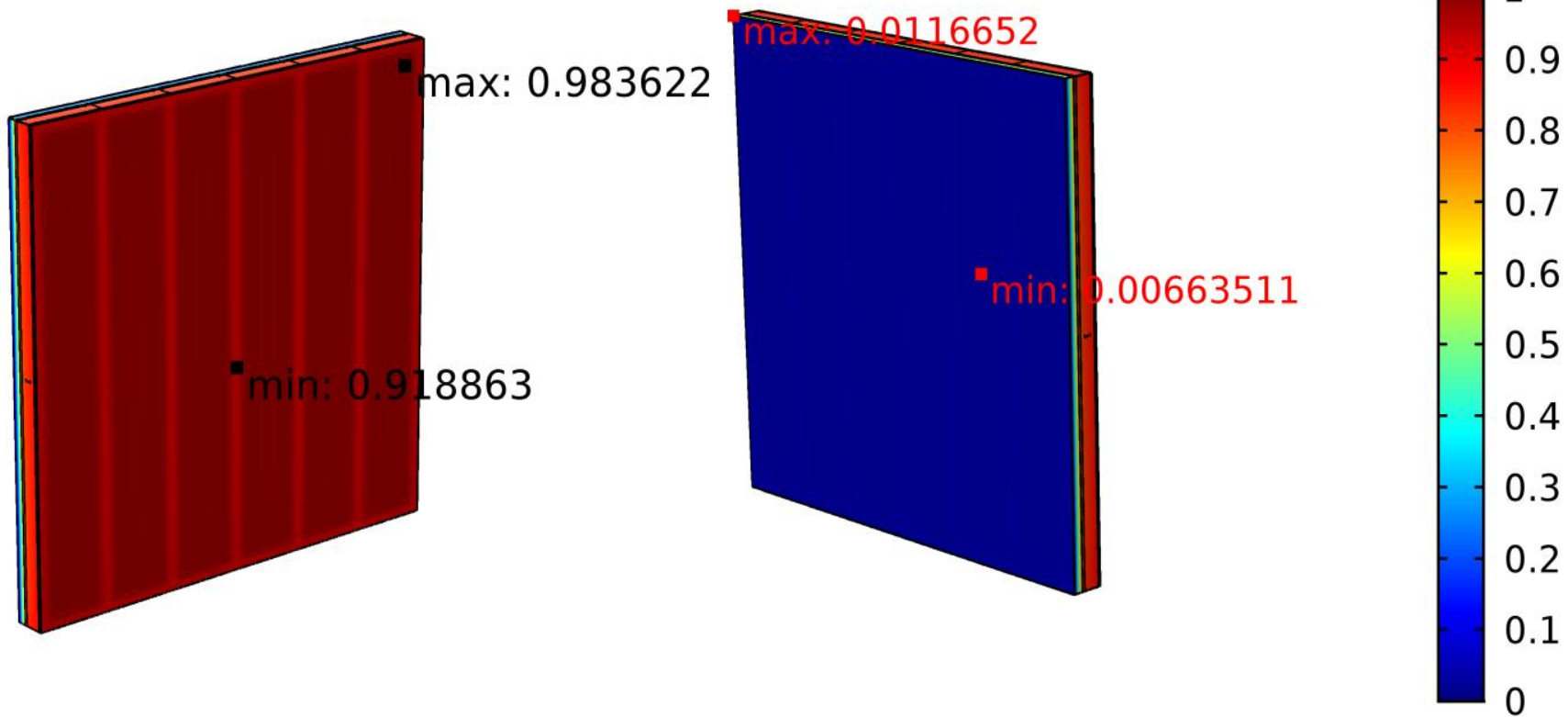
$$T_i = \frac{T_{surface} - T_{outdoor}}{T_{indoor} - T_{outdoor}}$$



W2 Surface Temperature Index

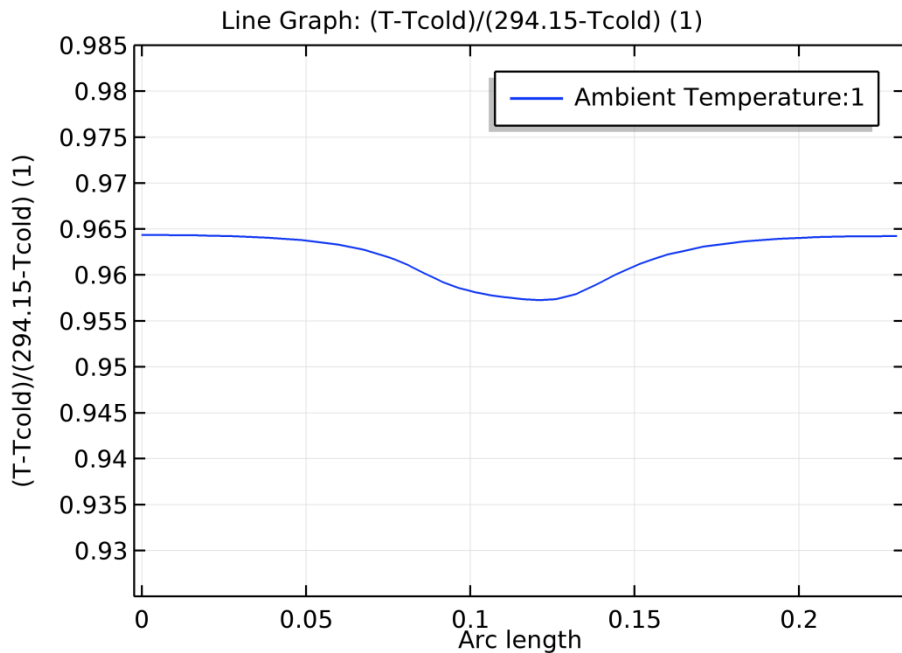


W3 Surface Temperature Index

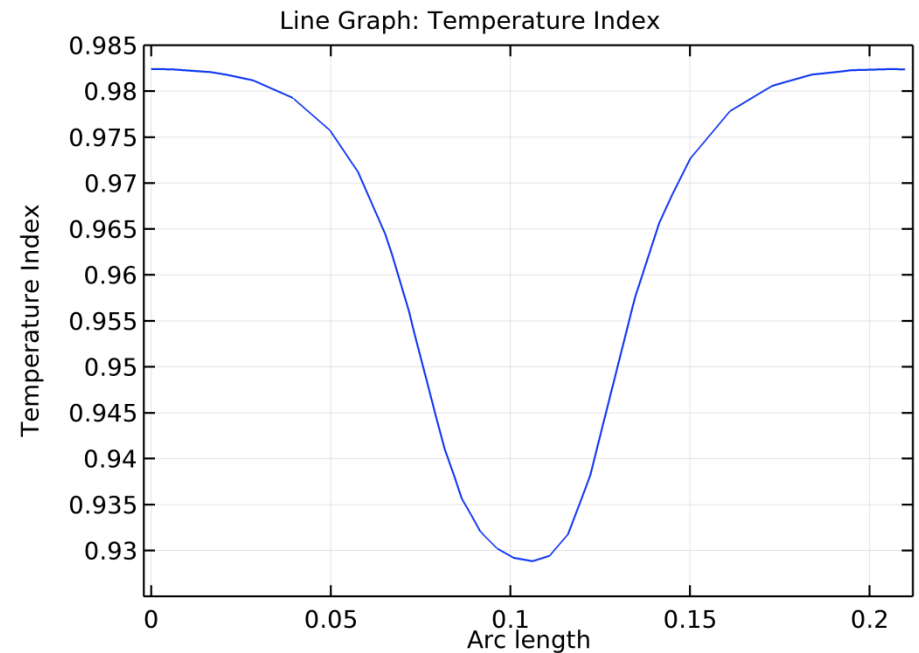


Temperature on the warm surface

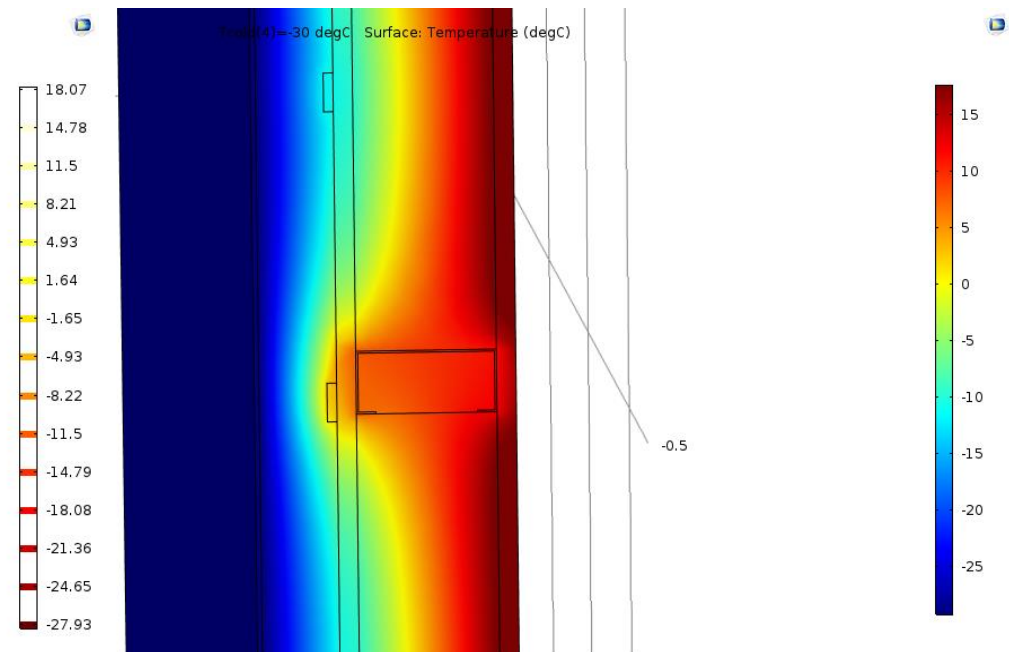
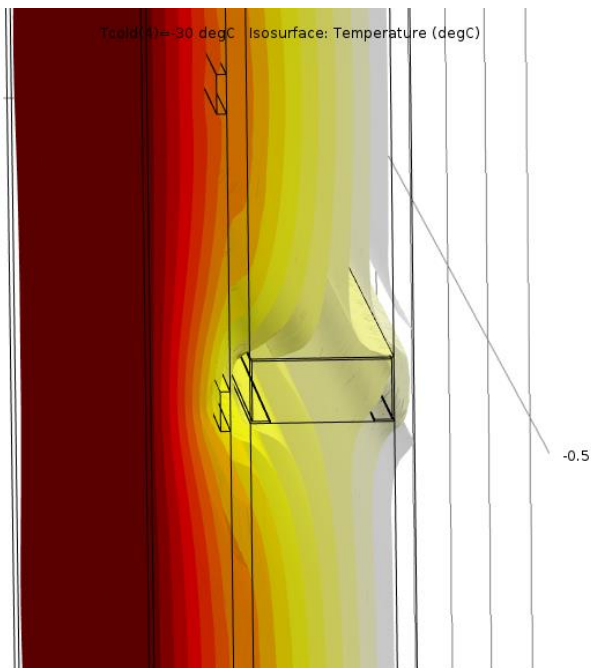
With exterior insulation



Without exterior insulation



W3. Temperature/isothermal surfaces along a stud



Benchmarking with the new GHB results

Benchmarking results for W1

| T_o (°C) | COMSOL results | | GHB Results | | | No Thermal Bridging | | |
|------------|----------------|-------|-------------|-------|--------------|---------------------|-------|-------------|
| | RSI StS | R StS | RSI StS | R StS | Difference | RSI StS | R StS | Increase |
| -5 | 1.36 | 7.77 | 1.43 | 8.17 | 5.13% | 2.82 | 16.02 | 106% |
| -20 | 1.37 | 7.73 | 1.42 | 8.30 | 3.55% | 3.03 | 17.20 | 122% |
| -35 | 1.45 | 8.14 | | | | 3.14 | 17.82 | 119% |

Benchmarking results for W2

| T_o (°C) | COMSOL results | | GHB Results | | | No Thermal Bridging | | |
|------------|----------------|-------|-------------|-------|--------------|---------------------|-------|------------|
| | RSI StS | R StS | RSI StS | R StS | Difference | RSI StS | R StS | Increase |
| -5 | 2.26 | 12.86 | 2.35 | 13.34 | 3.66% | 3.59 | 20.40 | 59% |
| -20 | 2.39 | 13.60 | 2.40 | 13.63 | 0.21% | 3.87 | 21.96 | 61% |
| -35 | 2.46 | 13.97 | 2.45 | 13.91 | 0.39% | 3.98 | 22.59 | 62% |

Benchmarking results for W3

| T_o (°C) | COMSOL results | | GHB Results | | | No Thermal Bridging | | |
|------------|----------------|-------|-------------|-------|--------------|---------------------|-------|------------|
| | RSI StS | R StS | RSI StS | R StS | Difference | RSI StS | R StS | Increase |
| -5 | 3.27 | 18.57 | 3.15 | 17.89 | 3.84% | 4.62 | 26.22 | 41% |
| -20 | 3.37 | 19.14 | 3.23 | 18.34 | 4.37% | 4.89 | 27.77 | 45% |
| -35 | 3.43 | 19.48 | 3.23 | 18.34 | 6.21% | 5.02 | 28.51 | 46% |

The importance of temperature dependent K

Benchmarking results for W1

| | Experimental results [5] | | MH Simulations [2] | | | COMSOL results | | |
|------------|--------------------------|---------|--------------------|---------|--------------|----------------|---------|--------------|
| T_o (°C) | RSI S-t-S | R S-t-S | RSI S-t-S | R S-t-S | Difference | RSI S-t-S | R S-t-S | Difference |
| -5 | 1.35 | 7.67 | 1.39 | 7.90 | 2.96% | 1.33 | 7.56 | 1.33% |
| -35 | 1.42 | 8.07 | 1.39 | 7.90 | 2.11% | 1.44 | 8.17 | 1.37% |

Benchmarking results for W2

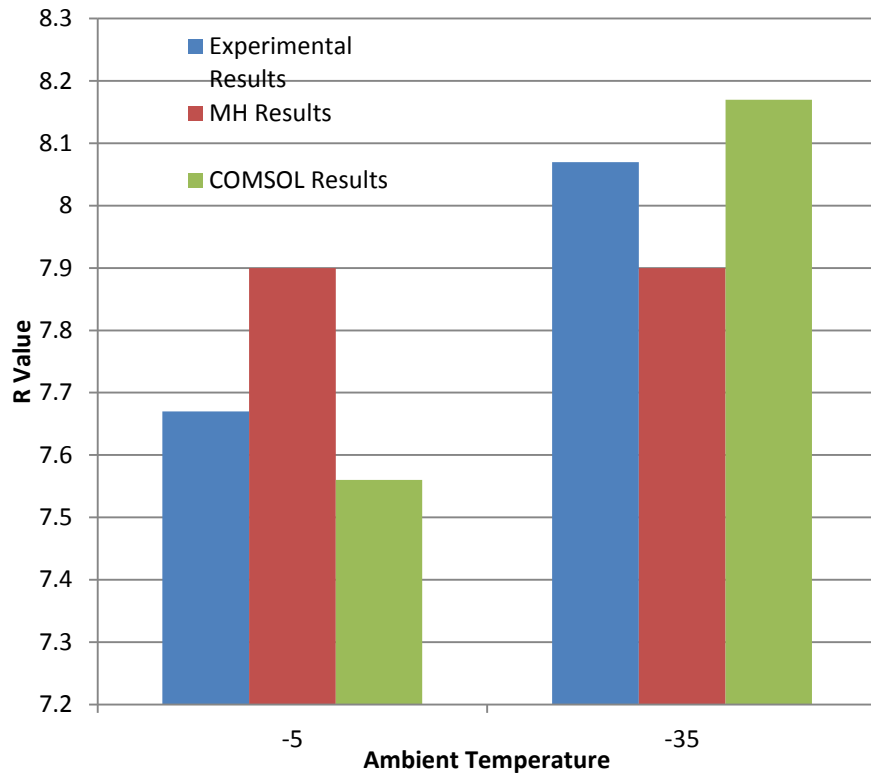
| | Experimental results [5] | | MH Simulations [2] | | | COMSOL results | | |
|------------|--------------------------|---------|--------------------|---------|--------------|----------------|---------|--------------|
| T_o (°C) | RSI S-t-S | R S-t-S | RSI S-t-S | R S-t-S | Difference | RSI S-t-S | R S-t-S | Difference |
| -5 | 2.29 | 13.00 | 2.38 | 13.51 | 3.93% | 2.31 | 13.10 | 0.71% |
| -35 | 2.41 | 13.68 | 2.38 | 13.51 | 1.24% | 2.44 | 13.86 | 1.29% |

Benchmarking results for W3

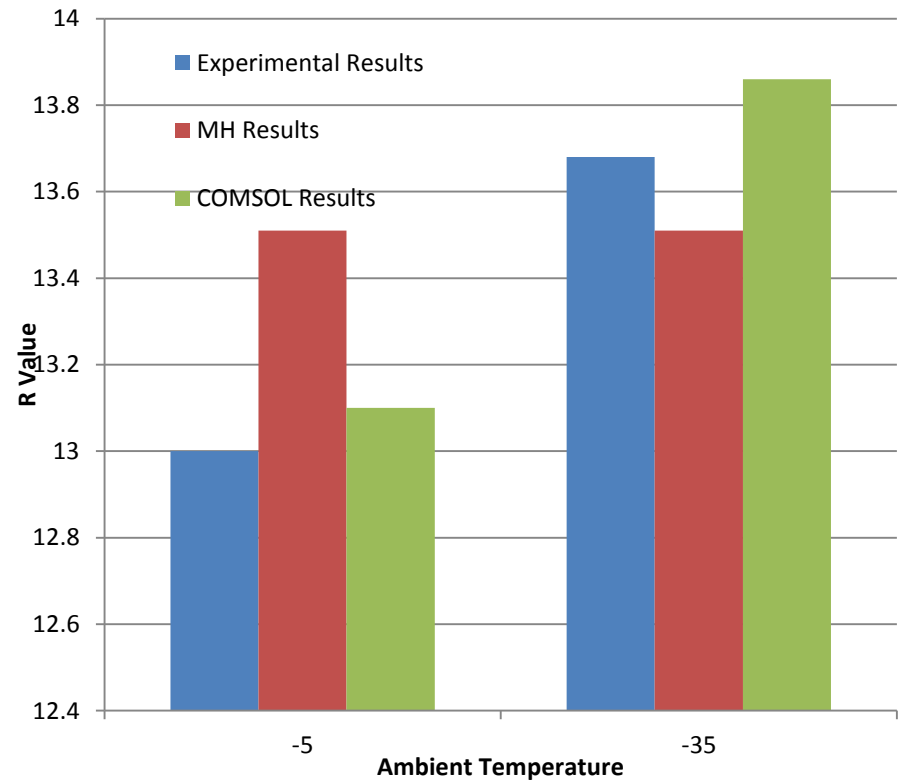
| | Experimental results [5] | | MH Simulations [2] | | | COMSOL results | | |
|------------|--------------------------|---------|--------------------|---------|--------------|----------------|---------|--------------|
| T_o (°C) | RSI S-t-S | R S-t-S | RSI S-t-S | R S-t-S | Difference | RSI S-t-S | R S-t-S | Difference |
| -5 | 3.09 | 17.55 | 3.30 | 18.74 | 6.80% | 3.20 | 18.18 | 3.56% |
| -35 | 3.29 | 18.68 | 3.30 | 18.74 | 0.30% | 3.42 | 19.45 | 3.95% |

The importance of temperature dependent K

Wall 1 comparison



Wall 1 comparison



Summary

- › Three wall assemblies from previous experimental studies were simulated in COMSOL and average differences of 1.35%, 1.00% and 3.75% were observed between our numerical results and the reported GHB results. All the values are within $\pm 8\%$ which is the uncertainty of GHB tests.
- › The wall assemblies were tested again in the NRC GHB facilities and another series of simulations were conducted and benchmarked against the results. Average differences of 4.34%, 1.42% and 4.80% were observed between our numerical results and the GHB results.
- › We also conducted another series of simulations replacing the thermal bridging material (steel) with the embedded insulation (glass-fiber) and calculated the R value increase. Average R value increases of 115%, 61% and 41% for the wall assemblies were found. It has been shown that the effect of thermal bridging can become less important by adding exterior insulation.
- › It has been shown that using high conductive materials within insulation materials can decrease the thermal performance of the wall more significantly.
- › Using the temperature dependent properties can highly affect the end results when the thermal properties of the used materials change with temperature.

Thank you for your attention.

Questions?

