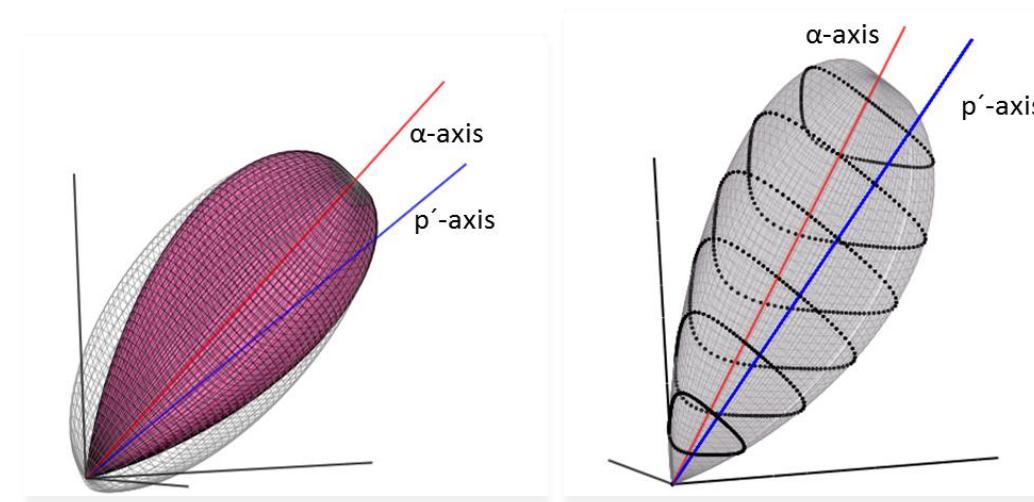


Implementation of a Modified Anisotropic Creep Model with Physics Builder

Structure for Soft Soils with the use of



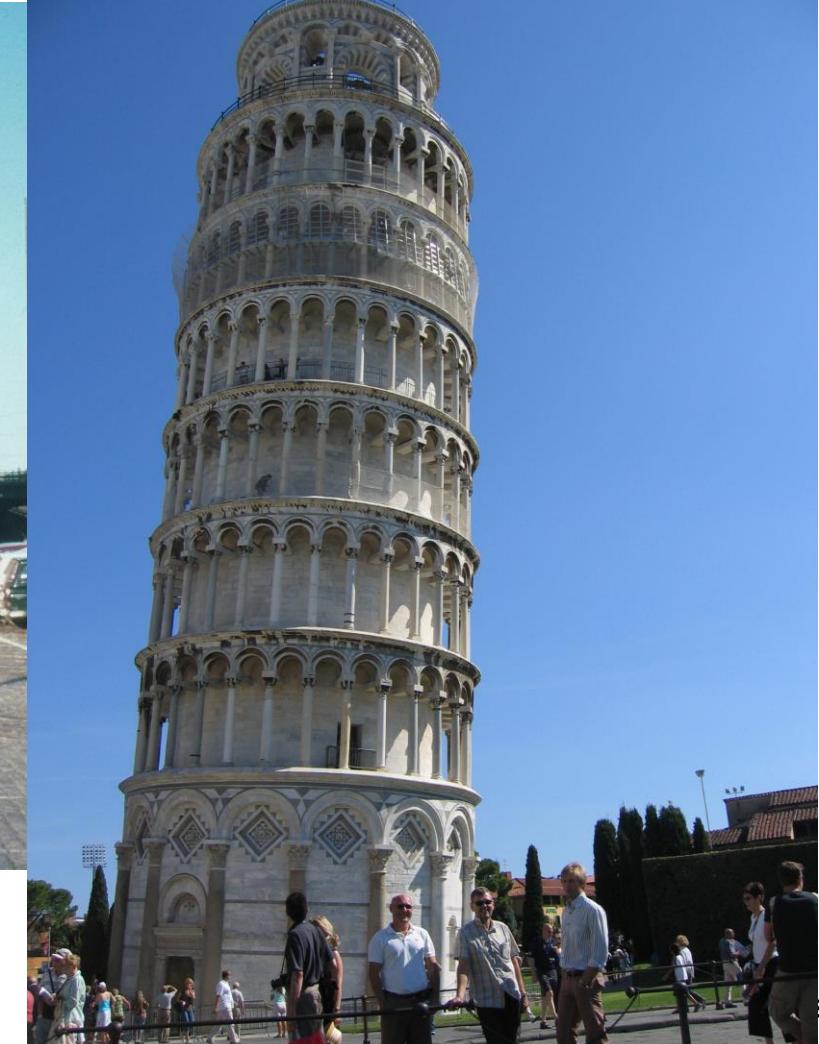
Mats Karlsson

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Outline

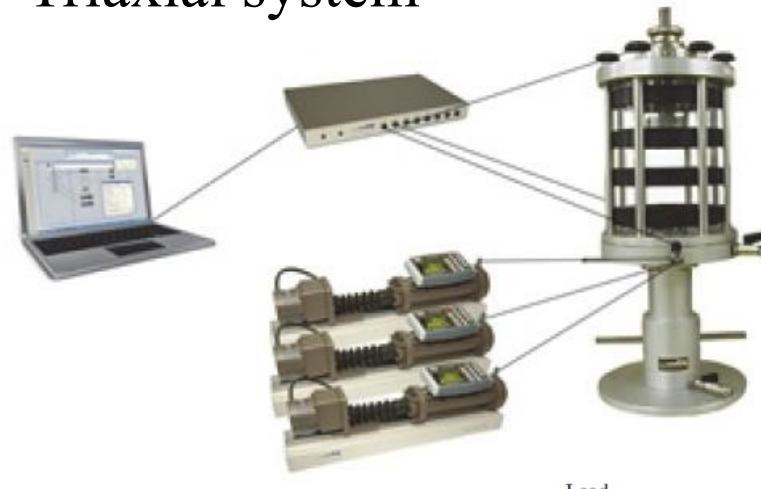
- Introduction
 - Creep/settlement in soft soils?
 - MAC-s model
- Physics builder
 - Implementation
 - GUI, input etc
- Validation of material model
 - Simulations
 - Example of real case

Building on Soft soils

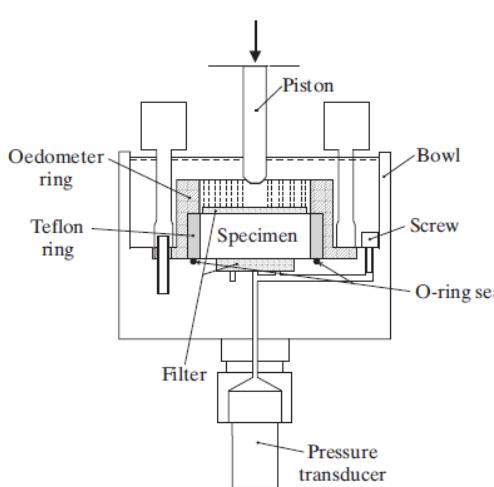


Soft soil behaviour

Triaxial system



Load
and
deformation transducer



Oedometer

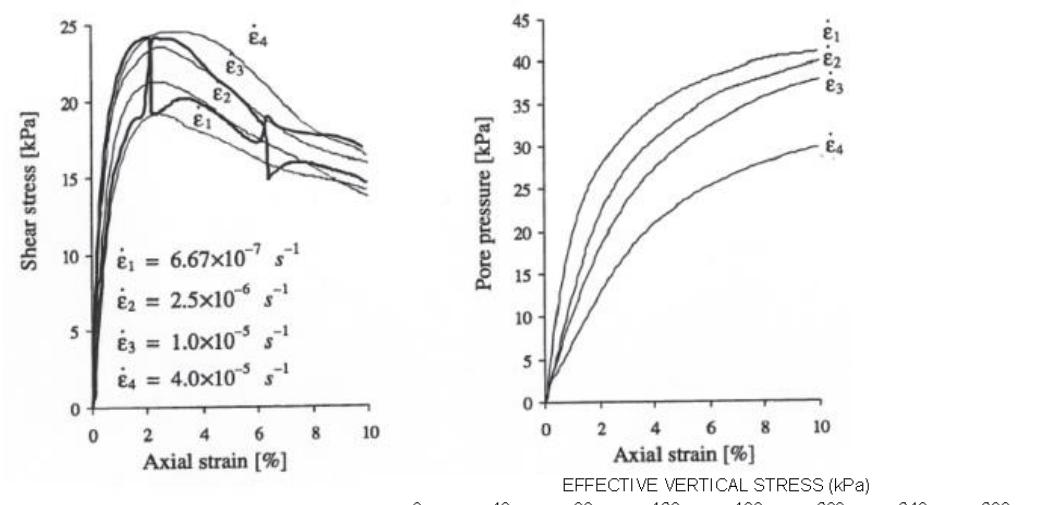
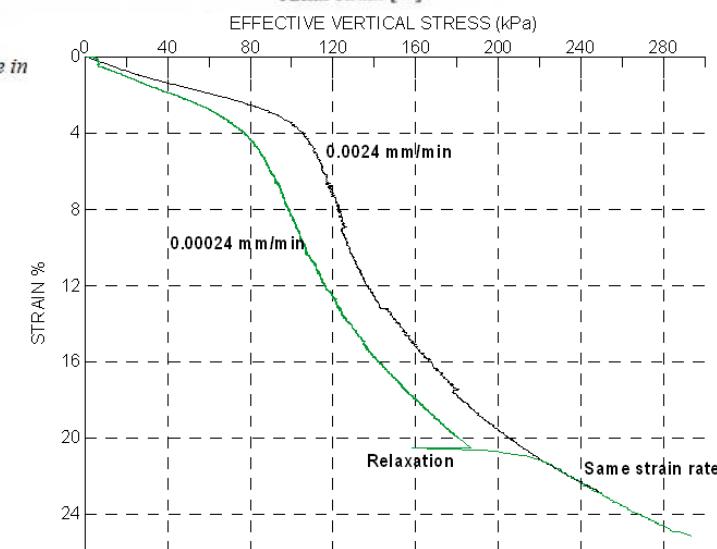


Figure 2.15. The effect of strain rate in
Länsivaara (1999)



Modified Anisotropic Creep model with structure (MAC-s)

$$p_{eq} = \frac{p'}{\left[1 - \frac{\frac{1}{2} \{ \boldsymbol{\sigma}_d - p' \cdot \mathbf{a}_d \}^T \{ \boldsymbol{\sigma}_d - p' \cdot \mathbf{a}_d \}}{p'^2 \cdot \left(M^2 - \frac{1}{2} \{ \mathbf{a}_d \}^T \{ \mathbf{a}_d \} \right)} \right]^{\frac{1}{m}}}$$

MAC-s (reference surface NCS)
Based on Grimstad (2009), Karstunen et.al (2005)

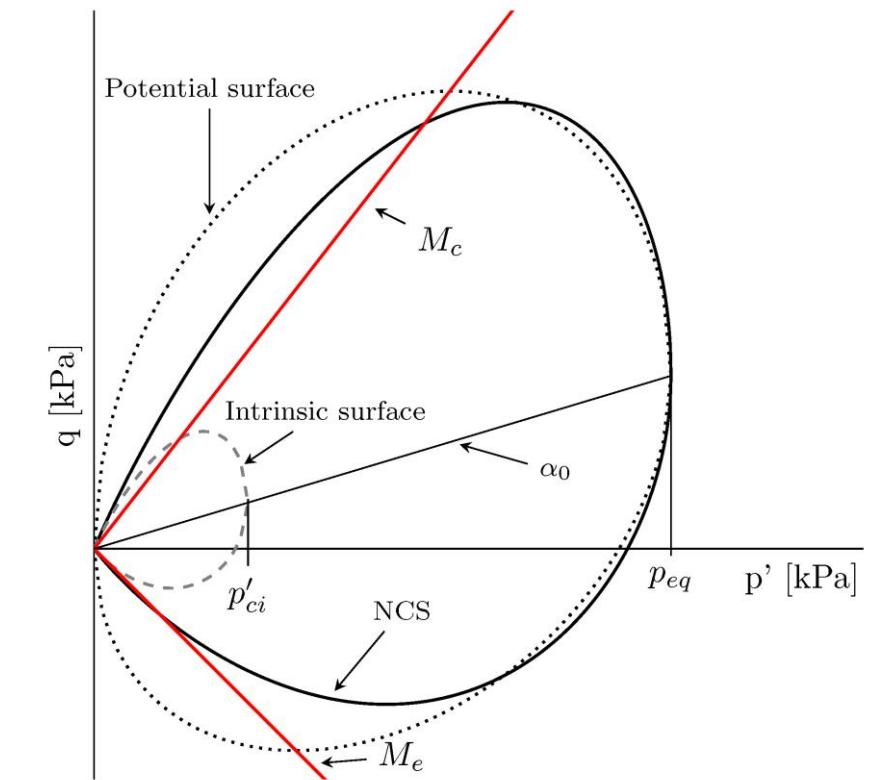
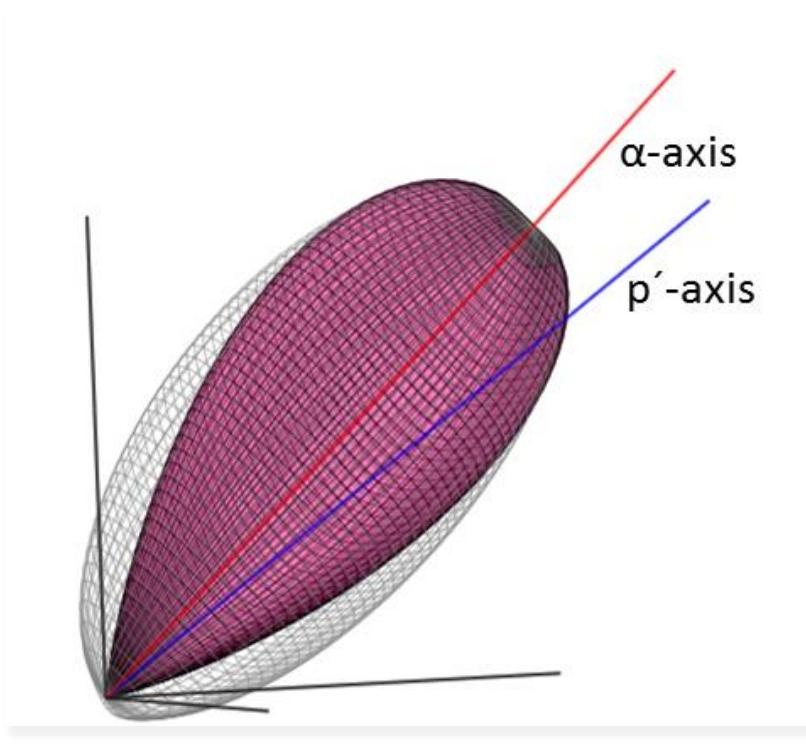
The plastic potential that is used for this model has the same shape as the CREEP-SCLAY1S model, i.e. the rotated ellipsoid

$$p_Q^{eq} = p' + \frac{3}{2} \cdot \frac{\{ \boldsymbol{\sigma}_d - p' \cdot \mathbf{a}_d \}^T \{ \boldsymbol{\sigma}_d - p' \cdot \mathbf{a}_d \}}{p' \left(M^2 - \frac{3}{2} \{ \mathbf{a}_d \}^T \{ \mathbf{a}_d \} \right)}$$

”Creep potential surface”

MAC-s model

- Graphical representation of the model



MAC-s model

- **Visco-plastic (rate) multiplier**

$$\dot{\lambda} = \frac{1}{r_{si} \cdot \tau} \cdot \left(\frac{p^{eq}}{(1+\chi) \cdot p'_{ci}} \right)^{r_{si} \cdot (\lambda_i^* - \kappa^*)} \cdot \frac{M_c^2 - \alpha_0^2}{M_c^2 - \eta_0^2}$$

Rotation of surfaces

$$d\mathbf{a}_d = \left(\omega_v \left[\frac{3\mathbf{\eta}}{4} - \mathbf{a}_d \right] \cdot \langle d\varepsilon_v^c \rangle + \omega_d^* \left[\frac{\mathbf{\eta}}{3} - \mathbf{a}_d \right] \cdot d\varepsilon_d^c \right)$$

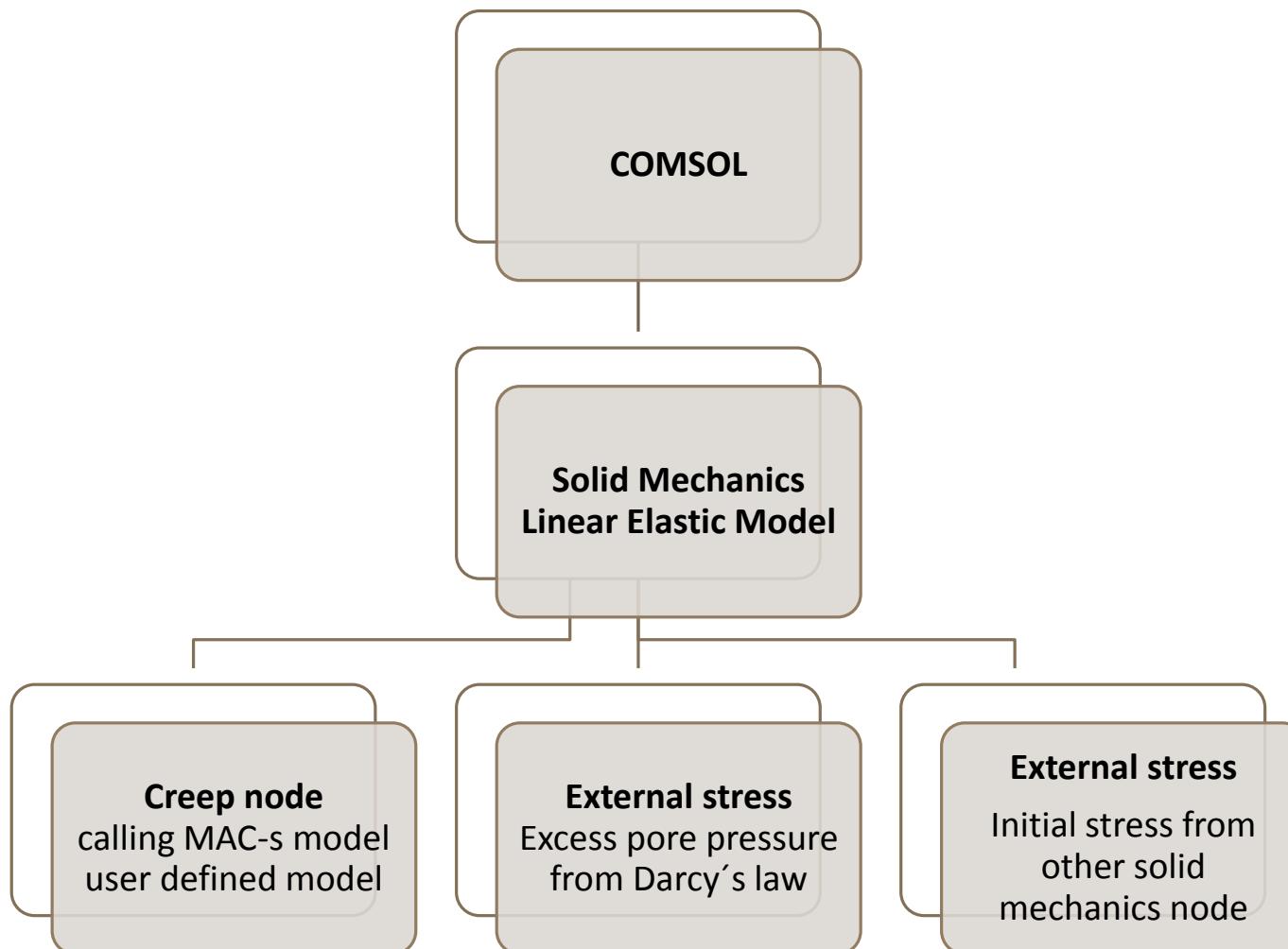
Change in size

$$p_{ci} = p_{ci0} \exp \left(\frac{\varepsilon_v^c}{\lambda_i^* - \kappa^*} \right)$$

Effect of structure

$$d\chi = -\chi \left(\xi_v |d\varepsilon_v^c| + \xi_d |d\varepsilon_d^c| \right)$$

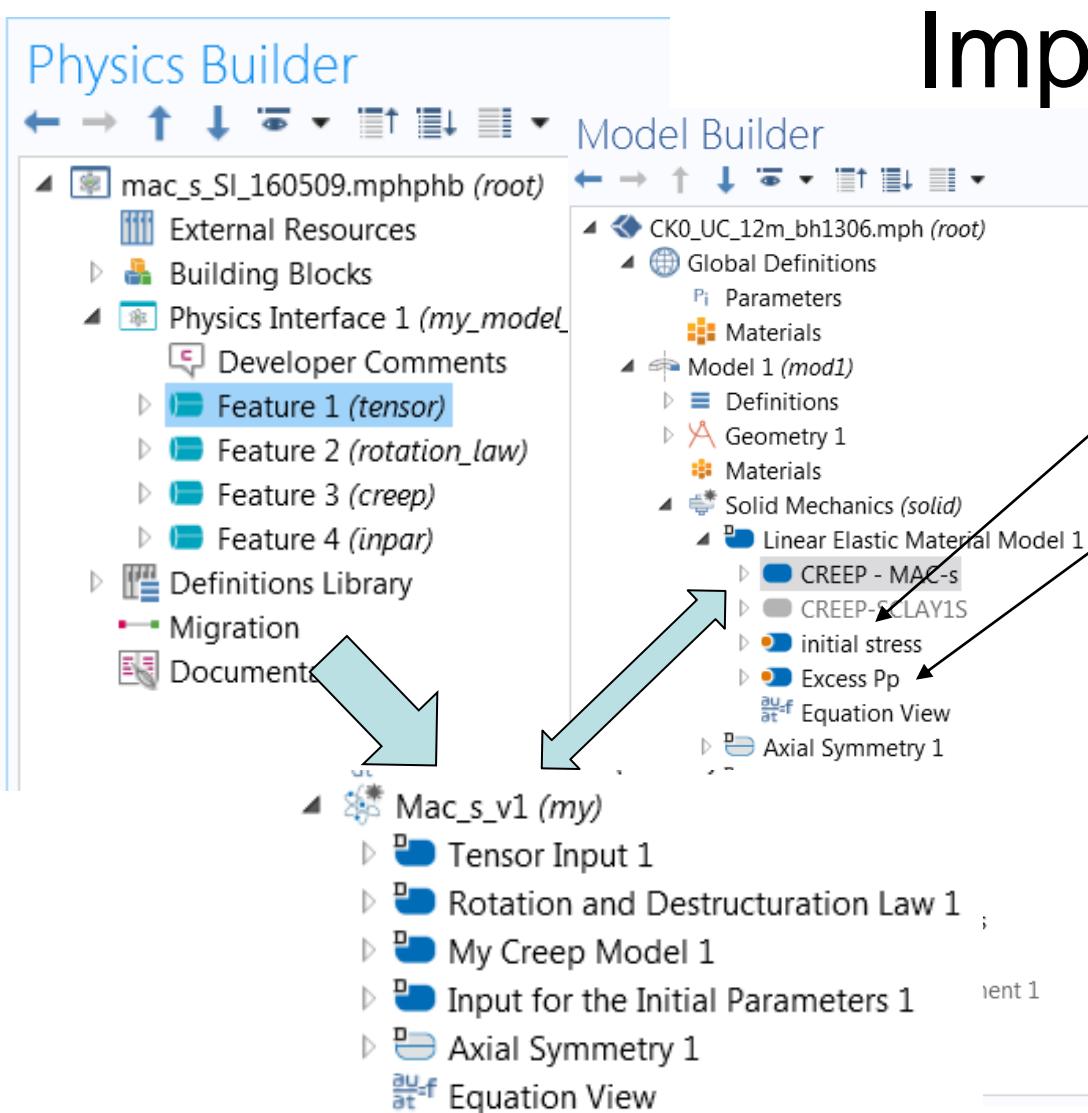
Implementation



Why?

- Make it easy to share
- Valid for all relevant dimensions
- General for any case
- Easy to adopt and change the equations

Implementation

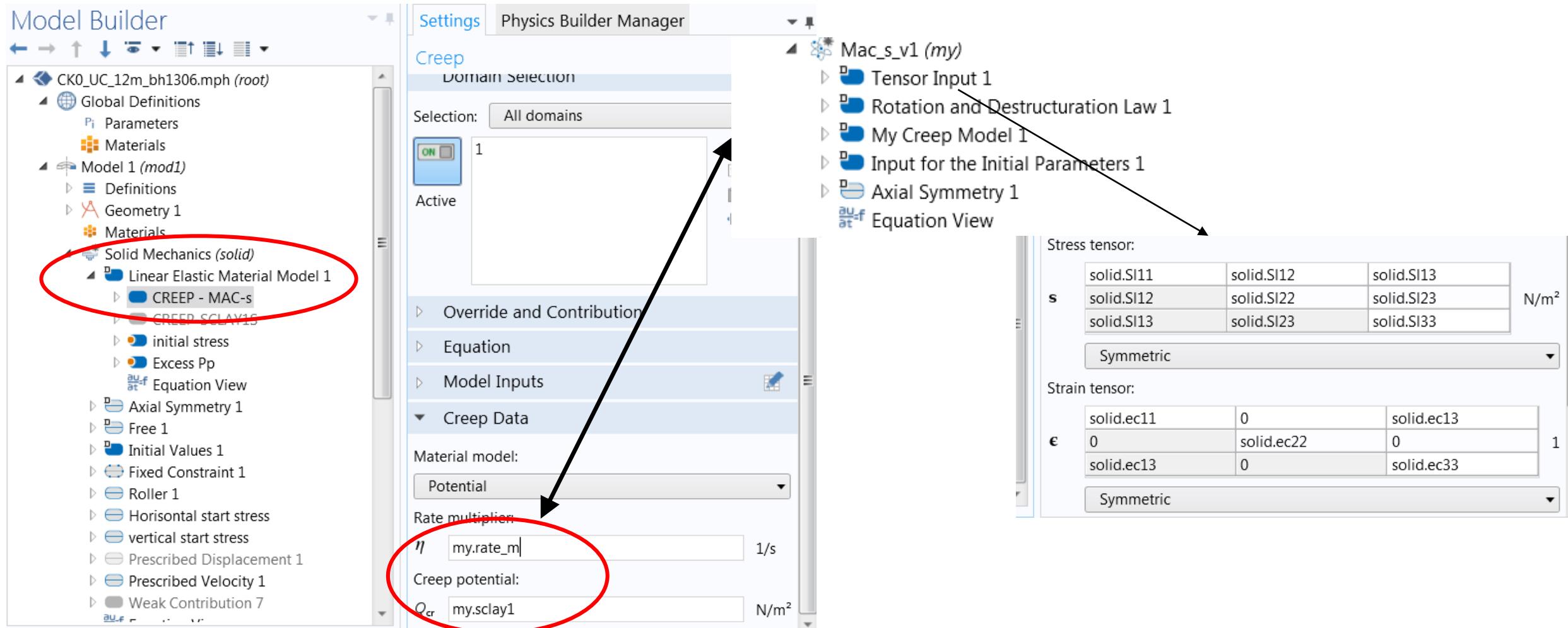


Initial stress calculated from another solid mechanics node (external stress input)

Excess pore pressure calculated in Darcy Law node (external stress pore pressure input)

- Darcy's Law (dl)
 - Fluid and Matrix Properties 1
 - Axial Symmetry 1
 - No Flow 1
 - Initial Values 1
 - Mass Source 1
 - Storage Model 1
 - Pressure 1
 - Equation View
- dl.rho*(d(solid.evol,TIME)) → Permeability etc

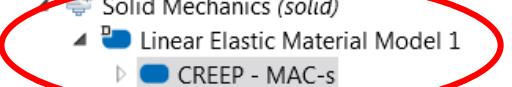
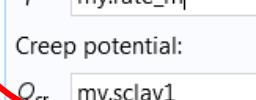
Implementation

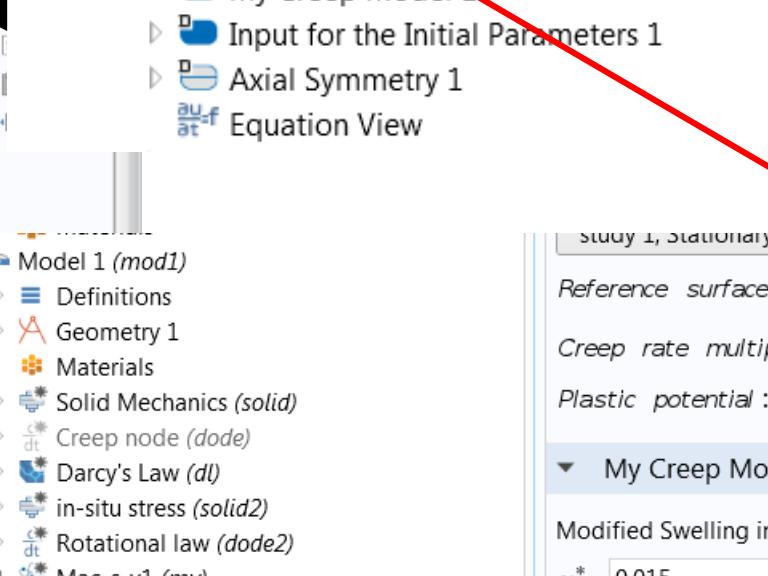


Implementation

Model Builder

- CK0_UC_12m_bh1306.mph (root)
 - Global Definitions
 - Parameters
 - Materials
 - Model 1 (mod1)
 - Definitions
 - Geometry 1
 - Materials
 - Solid Mechanics (solid)
 - Linear Elastic Material Model 1
 - CREEP - MAC-s
 - CREEP SCLAY15
 - initial stress
 - Excess Pp
 - Equation View
 - Axial Symmetry 1
 - Free 1
 - Initial Values 1
 - Fixed Constraint 1
 - Roller 1
 - Horizontal start stress
 - vertical start stress
 - Prescribed Displacement 1
 - Prescribed Velocity 1
 - Weak Contribution 7



Settings Physics Builder Manager

Creep

Domain Selection

Selection: All domains

Active

Override and Contribution

Equation

Model Inputs

Creep Data

Material model: Potential

Rate multiplier: η my.rate_m

Creep potential: Q_{cr} my.sclay1

Mac_s_v1 (my)

- Tensor Input 1
- Rotation and Destructuration Law 1
- My Creep Model 1
- Input for the Initial Parameters 1
- Axial Symmetry 1
- Equation View

STUDY 1, STATIONARY

Reference surface: $P_{eq} = p_{eff}/(1 - J2^{\alpha}/(p_{eff}^2 \cdot (M(\theta)^2 - 0.5 \cdot \alpha_d : \alpha_d)))^{1/m}$

Creep rate multiplier: $\eta = 1/(r_{si} \cdot \tau) \cdot (P_{eq}/P_c)^{(\lambda^* - \kappa^*) \cdot r_{si}} \cdot m \cdot k \cdot \Omega \cdot c$

Plastic potential: $P_{eq}^0 = 3 \cdot J2^{\alpha} - (M(\theta)^2 - 3/2 \cdot \alpha_d : \alpha_d) \cdot (p_c - p_{eff}) \cdot p_{eff}$

My Creep Model

Modified Swelling index: κ^* 0.015

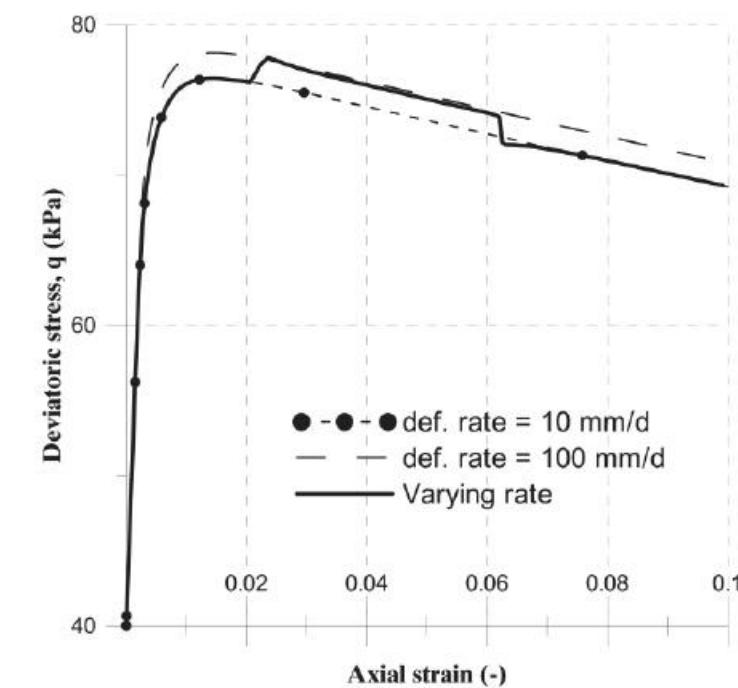
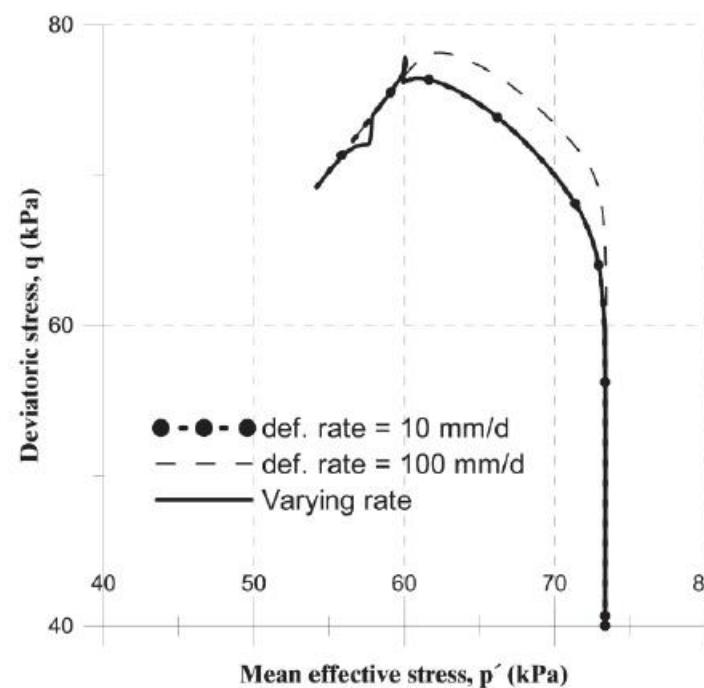
Modified Compression index (intrinsic): λ_i^* 0.097

Reference time (day): τ 1[d]



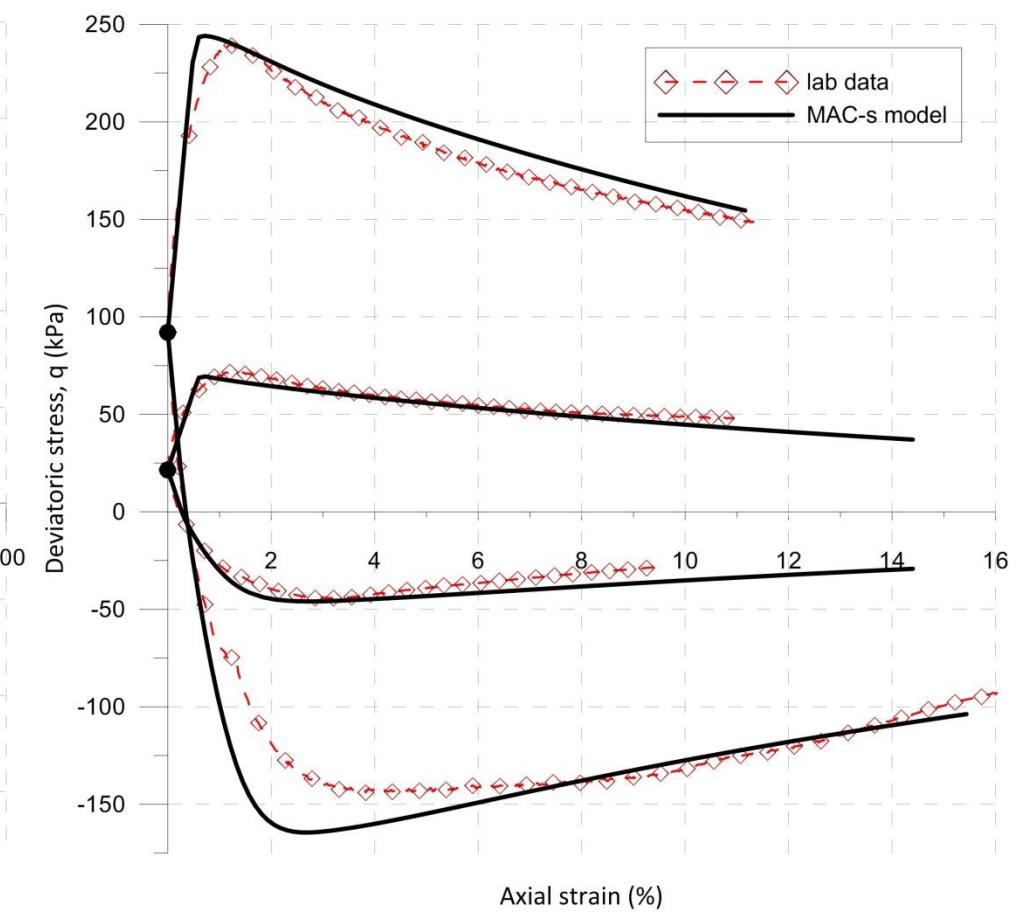
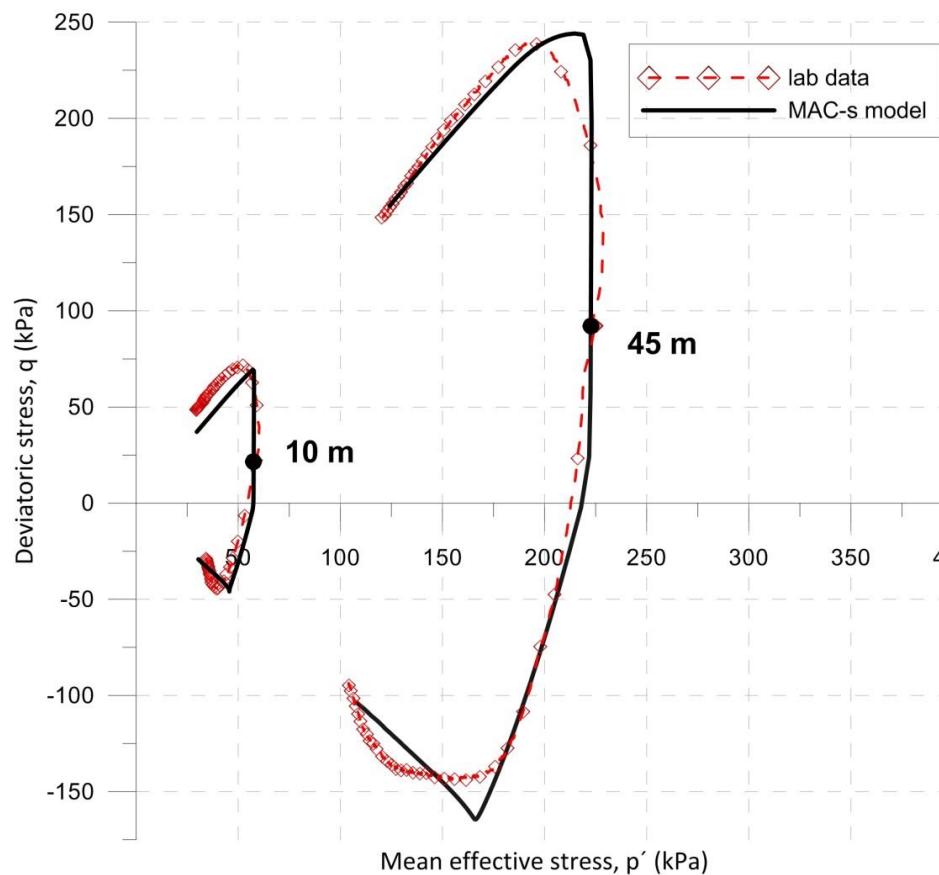
Simulations

Undrained triaxial test - compression



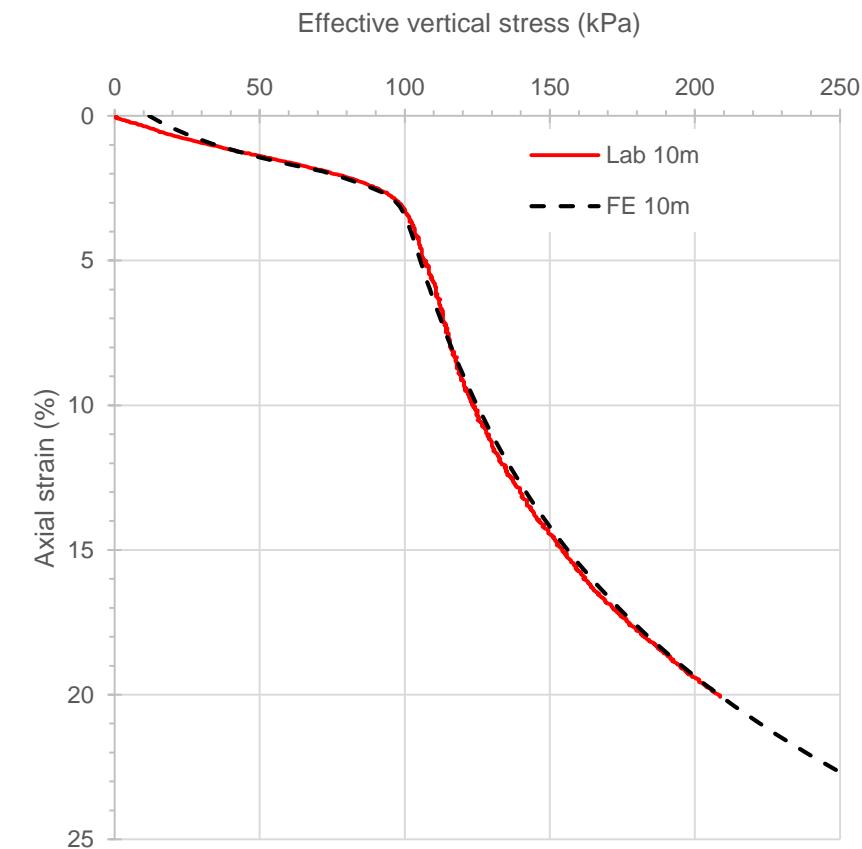
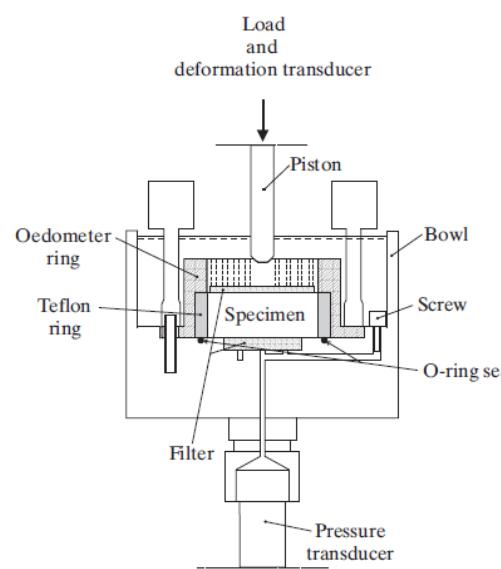


Simulations – triaxial tests

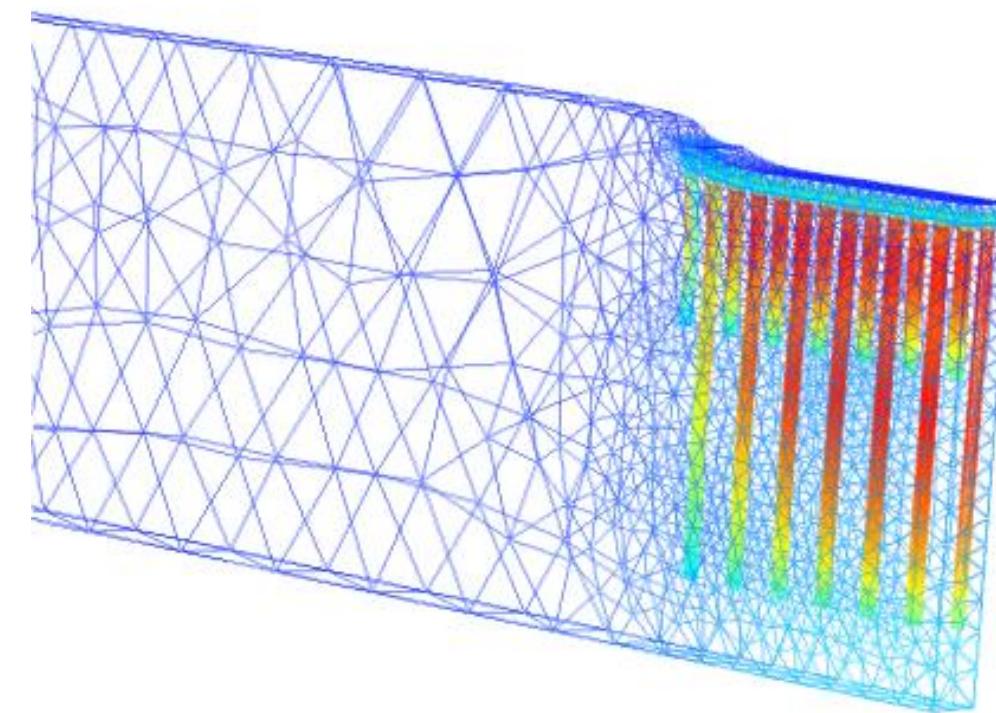


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Simulations – Oedometer test



Real case – Road embankment Lime-Cement Column reinforcement



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**Thank you
for
your attention**