



# Mitigation of Greenhouse Gas Leakage from Oil and Gas Wells

H. Spencer, Seal Well Inc.

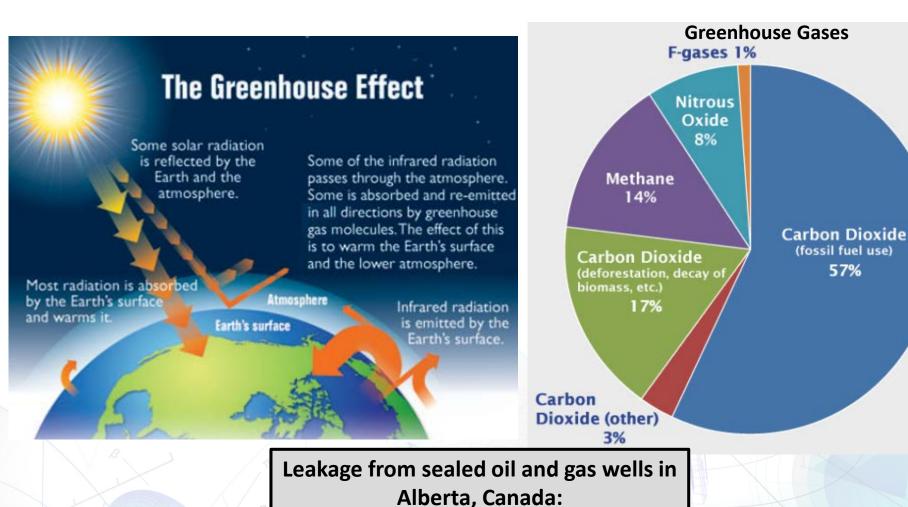
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**AltaSim Technologies** 

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## Background



~3.5 million tonnes GHG per year 14% of sealed wells leak



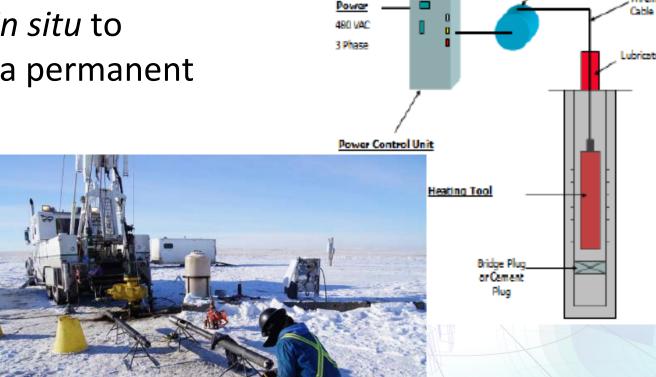
#### **Seal Well Technology**

Alloy Plugging Process\*

- Low melting point bismuth-tin alloy
- Molded in situ to produce a permanent seal

\*Process and Heating Tool covered by various issued and pending.

Spool

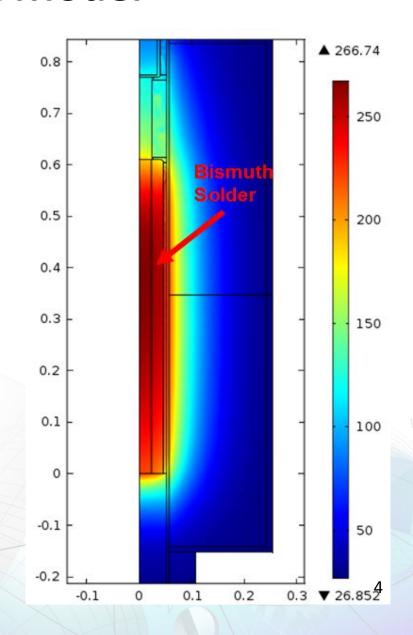


Input



#### **COMSOL Model**

- Heating to melt the bismuth-tin alloy in sufficient volume to infiltrate the porous structure around the well head
- Development of a stress distribution with sufficient strength to provide a permanent seal.





#### **COMSOL Model**

- Heat Transfer
  - Conduction
  - Phase change
- Fluid flow
  - Conjugate heat transfer
  - Convection
- Structural mechanics
  - Isotropic hardening plasticity

$$\rho \ c_p \frac{\partial T}{\partial t} = \nabla \cdot (\lambda \nabla T)$$

$$\nabla \cdot (\rho \mathbf{u}) = 0$$

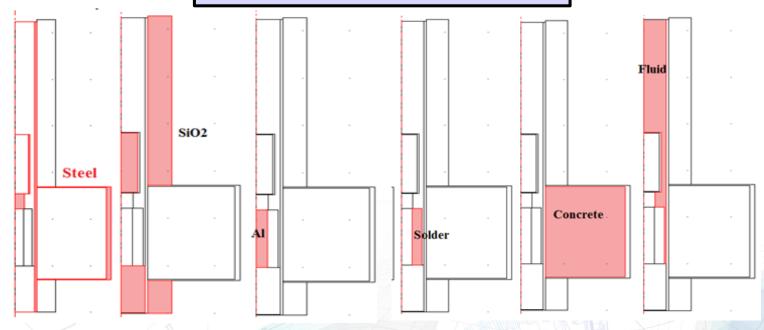
$$\rho \mathbf{u} \cdot \nabla \mathbf{u} = -\nabla p + \nabla \cdot \left( \eta (\nabla \mathbf{u} + (\nabla \mathbf{u})^T) - \frac{2}{3} \eta (\nabla \cdot \mathbf{u}) \mathbf{I} \right) + \rho \mathbf{g}$$

$$\nabla \cdot (-k \nabla T) = Q - \rho c_p \mathbf{u}$$

ructural mechanics | 
$$\nabla \bullet \sigma = 0$$
 | Isotropic hardening |  $\sigma = C : \varepsilon_{el}$  |  $\varepsilon^T = \varepsilon_{el} + \varepsilon_{th}$  |  $\varepsilon_{th} = \alpha_{th} (T - T_{ref})$ 

## **COMSOL Model - Heating**

Axisymmetric model
Multiple material domains
Heater unit in place

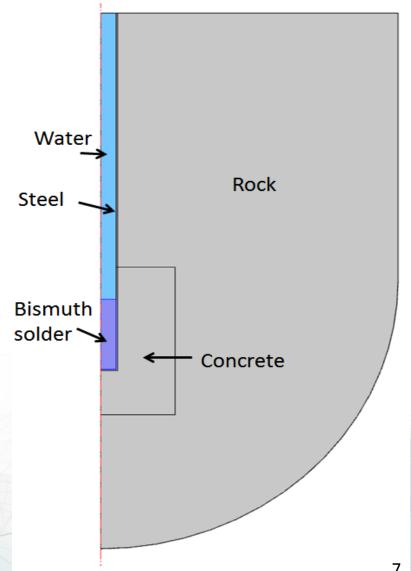




Heat transfer Fluid mechanics

## **COMSOL Model - Cooling**

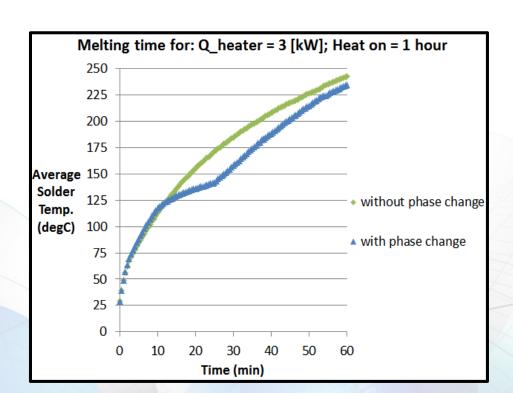
- Axisymmetric model showing material domain
- Heater unit removed
- Liquid bismuth-tin solder pools at the bottom of the well
  - Heat transfer
  - Structural mechanics

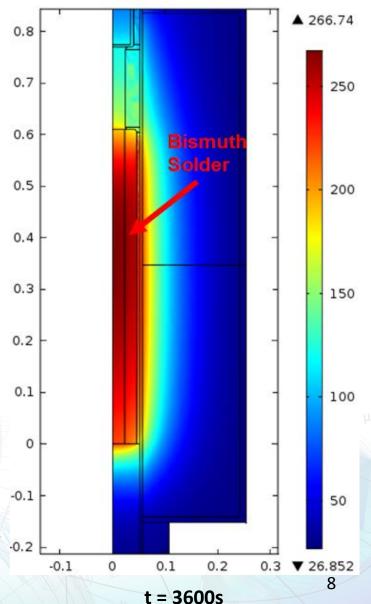




#### **Results: Heating**

- Temperature vs time
- Temperature distribution
- Process conditions





**Results: Cooling** ▲ 74.829 ▲ 0.274 **Von Mises stress Plastic strain** 0.64 0.64 0.014 0.62 0.62 18 0.6 0.6 **Residual stress/strain** 0.58 0.012 0.58 distribution in well 0.56 0.56 seal region 0.54 0.01 0.54 12 0.52 0.52 0.008 0.5 0.5 10 0.48 0.48 0.006 0.46 0.46 0.44 0.44 0.004 0.42 0.42 240 0.4 Max. Temp in Bi solder plug (degC) 220 0.002 Min. Temp in Bi solder plug (degC) 0.38 200 Av. Radial Stress at Interface (comp. +) (MPa) 0.36 180 0.05 0 0.05 **▼** 0 -0.05 0.05 160 T=137°C (freezing point) Liquid 140 Solid 120 100 80 60 40 Final Ave. Radial Stress at interface 20 9 0 3

Time (h)

#### Summary

- Computational model of Seal Well's technology for sealing GHG emitting wells has been used for:
  - Development of effective processing parameters
  - Identification of solidification induced residual stresses
- Seal Well technology currently under demonstration and implementation



Boundary conditions:

Conjugate heat transfer:
No slip velocity at all walls,
pressure point constraint at
about 2.5 meters in the vertical
direction from the bottom of
the water column, Fixed rock
temperature at a circular radius
of 4 meters away from unit in
rock formation.

See following slides

Typical Model size:

100k DoF

Heat Transfer step: 4k DoF Solid Mechanics step: 26k DoF

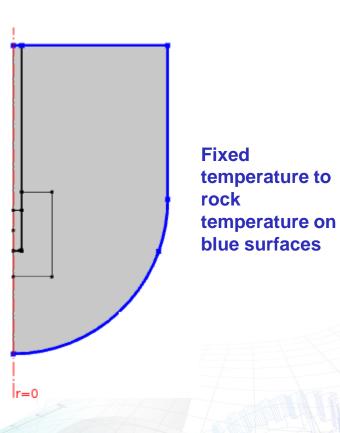
Typical Run times:

17 hours of walltime for 1 hour of simulation time to completely melt the alloy

Heat Transfer step: 0.5 hours Solid Mechanics step: 5 hours



# Model with heater removed (Heat Transfer boundary conditions)





# Model with heater removed (Solid mechanics boundary conditions)

