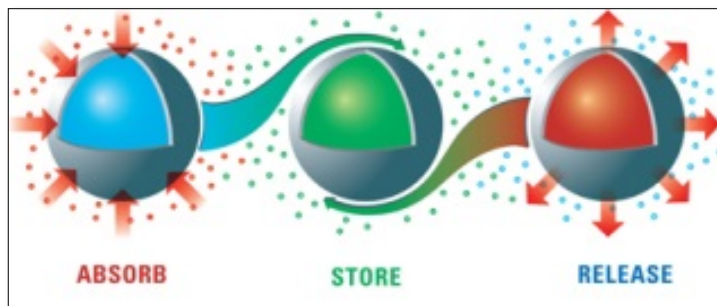


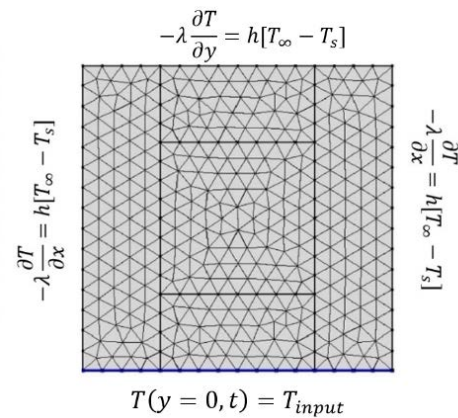
COMSOL Modeling of Temperature Changes in Building Materials Incorporating Phase Change Materials

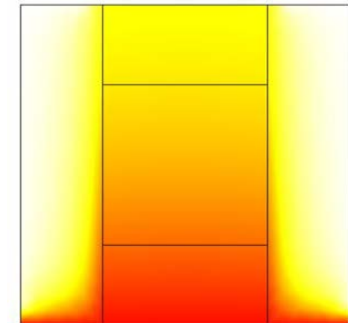


$$-\lambda \frac{\partial T}{\partial y} = h[T_{\infty} - T_s]$$

$$-\lambda \frac{\partial T}{\partial x} = h[T_{\infty} - T_s]$$

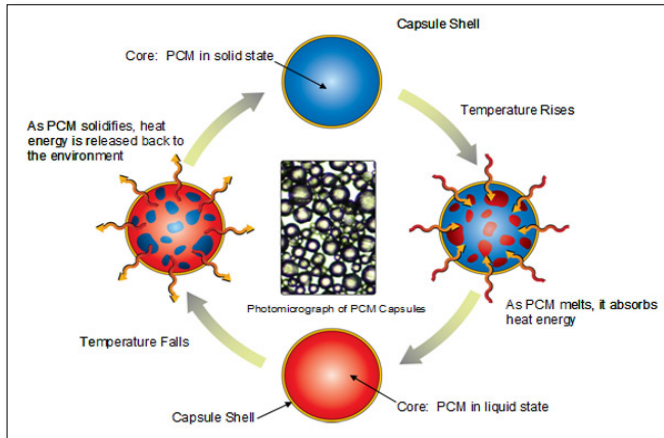
$$-\lambda \frac{\partial T}{\partial x} = h[T_{\infty} - T_s]$$

$$T(y = 0, t) = T_{input}$$




Naser P. Sharifi, Ahsan A. N. Shaikh, Aaron R. Sakulich

1- PCMs



2- COMSOL Modeling

Equation

Show equation assuming:

Study 1, Time Dependent

$$d_z \rho C_p \frac{\partial T}{\partial t} + d_z \rho C_p \mathbf{u} \cdot \nabla T = \nabla \cdot (d_z k \nabla T) + d_z Q + Q_{vd} + Q_p + Q_{oop}$$

$$\rho = \theta \rho_{phase1} + (1 - \theta) \rho_{phase2}$$

$$C_p = \frac{1}{\rho} (\theta \rho_{phase1} C_{p,phase1} + (1 - \theta) \rho_{phase2} C_{p,phase2}) + L \frac{\partial \alpha_m}{\partial T}$$

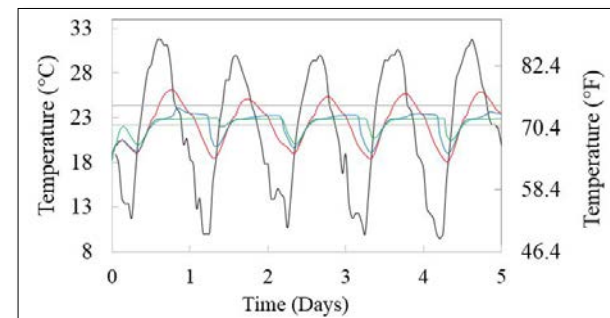
$$k = \theta k_{phase1} + (1 - \theta) k_{phase2}$$

$$\alpha_m = \frac{1}{2} \frac{(1 - \theta) \rho_{phase2} - \theta \rho_{phase1}}{\theta \rho_{phase1} + (1 - \theta) \rho_{phase2}}$$

3- Model Validating



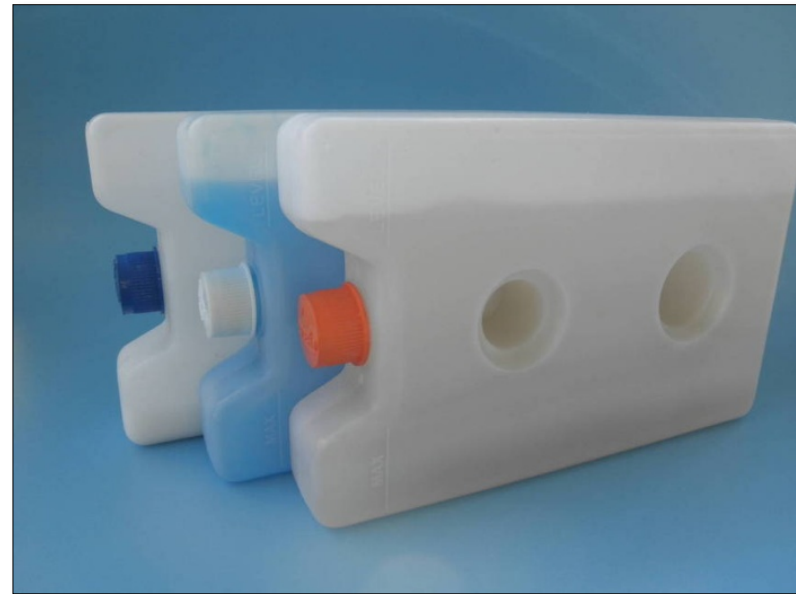
4- Actual Results



- Phase Change Materials:
 - Specific melting point
 - High latent heat of fusion

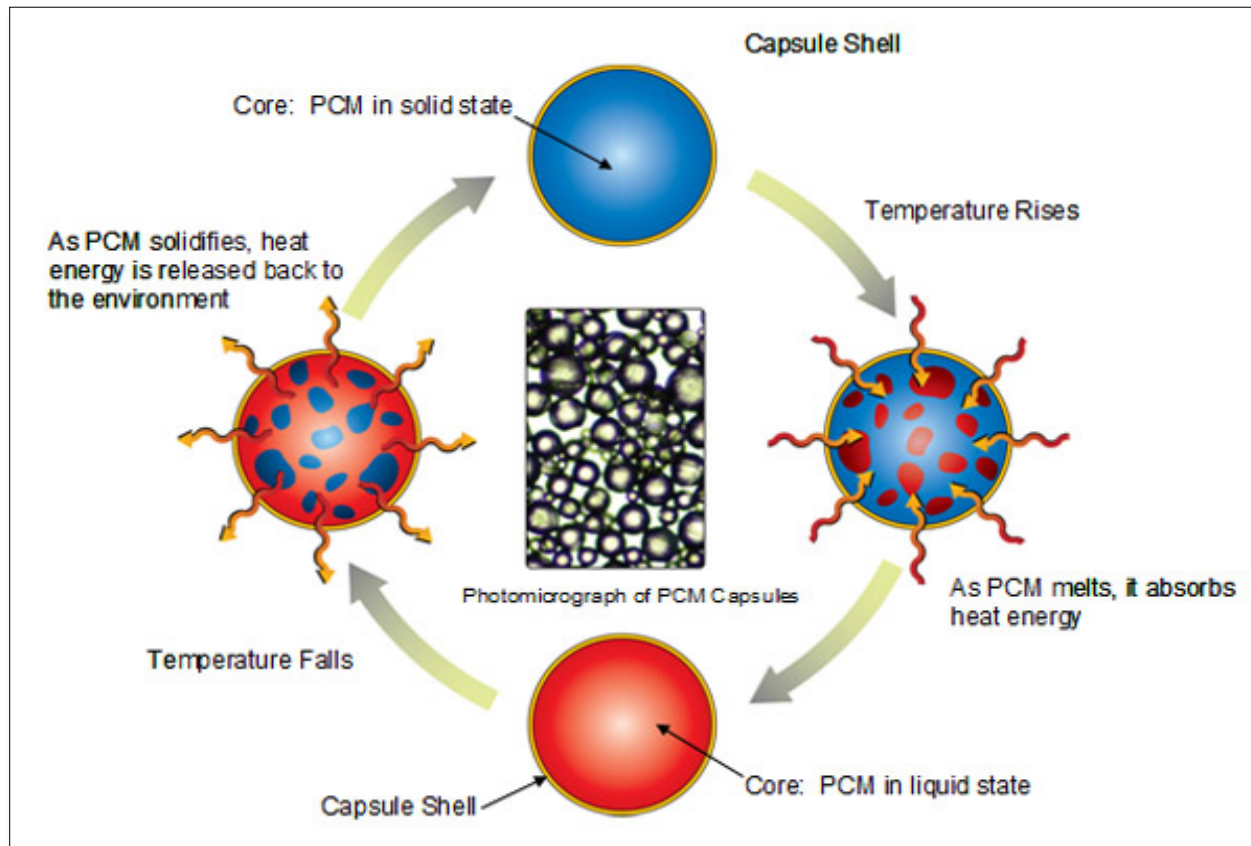


<http://www.pcmproducts.net>



<http://www.thomasnet.com>

- Absorbs heat; Temperature remains constant



- PCMs are passive interior heat energy storage units

Material	Melting Point	Latent Heat
	°C (°F)	kJ/kg (cal/g)
SN26	-26 (-14.8)	268 (64.0)
SN15	-11 (12.2)	311 (74.3)
SN06	-6 (21.2)	286 (68.3)
RT5	9 (48.2)	205 (48.9)
RT25	26 (78.8)	232 (55.4)
RT50	54 (129.2)	195 (46.6)
RT90	90 (194.0)	197 (47.1)

- Desire for more energy efficient buildings
- Increase occupant comfort
- Environmentally friendly construction



<http://www.dranguell.com>

The question is:

- What is the best Melting Temperature for buildings that are located in different cities?
- What is the optimum PCM percentage?
- How effective is the PCM?
- How much energy of HVAC system will be saved?



Using COMSOL to model temperature changes in structural elements

Step 1: Modeling porous media and PCM

Step 2: Validating the Model

Step 3: Using real temperature profiles of different cities

Equation

Show equation assuming:

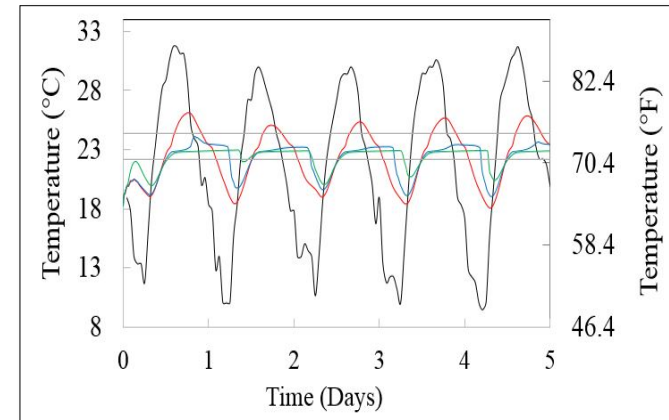
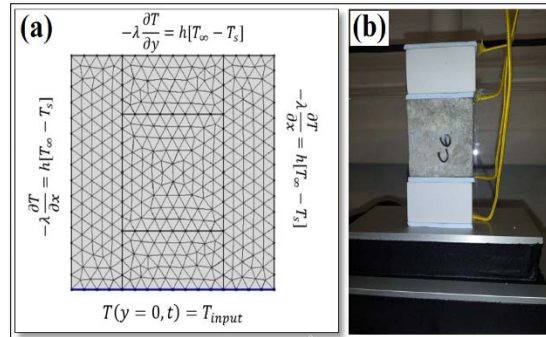
Study 1, Time Dependent

$$d_z \rho C_p \frac{\partial T}{\partial t} + d_z \rho C_p \mathbf{u} \cdot \nabla T = \nabla \cdot (d_z k \nabla T) + d_z Q + Q_{vd} + Q_p + Q_{oop}$$

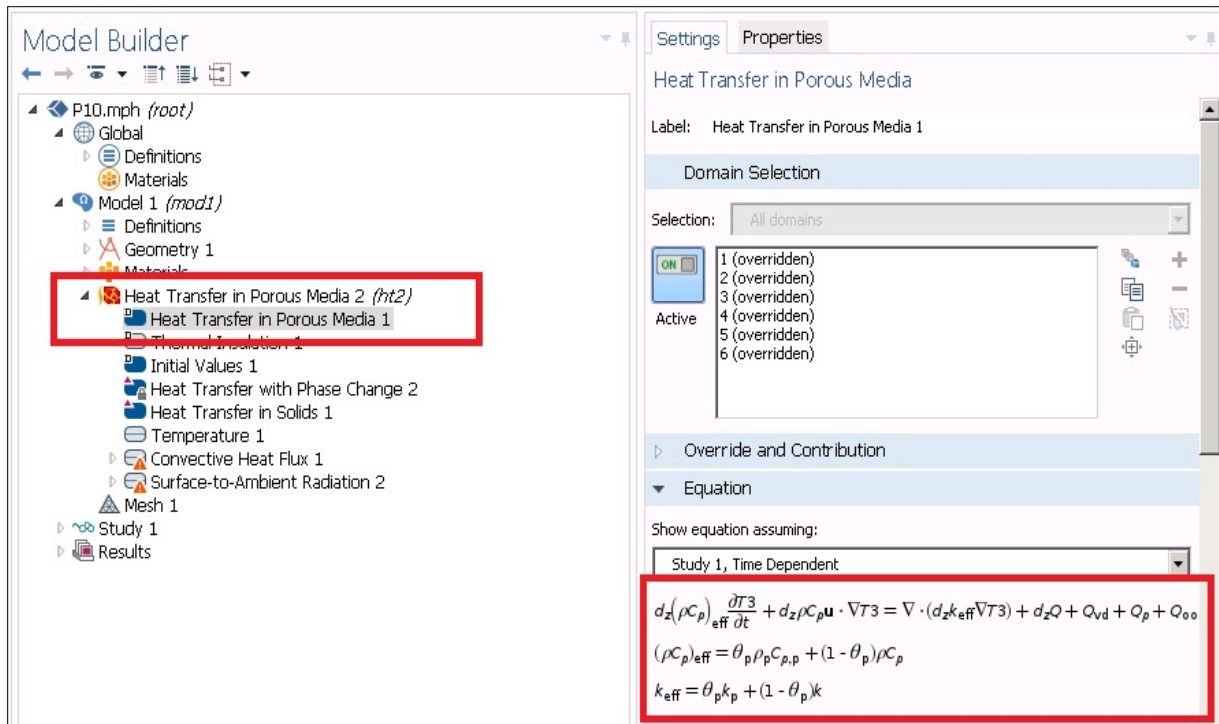
$$\rho = \theta \rho_{\text{phase1}} + (1 - \theta) \rho_{\text{phase2}}$$

$$C_p = \frac{1}{\rho} (\theta \rho_{\text{phase1}} C_{p,\text{phase1}} + (1 - \theta) \rho_{\text{phase2}} C_{p,\text{phase2}}) + L \frac{\partial \alpha_m}{\partial T}$$

$$k = \theta k_{\text{phase1}} + (1 - \theta) k_{\text{phase2}}$$

$$\alpha_m = \frac{1}{2} \frac{(1 - \theta) \rho_{\text{phase2}} - \theta \rho_{\text{phase1}}}{\theta \rho_{\text{phase1}} + (1 - \theta) \rho_{\text{phase2}}}$$


Porous Media

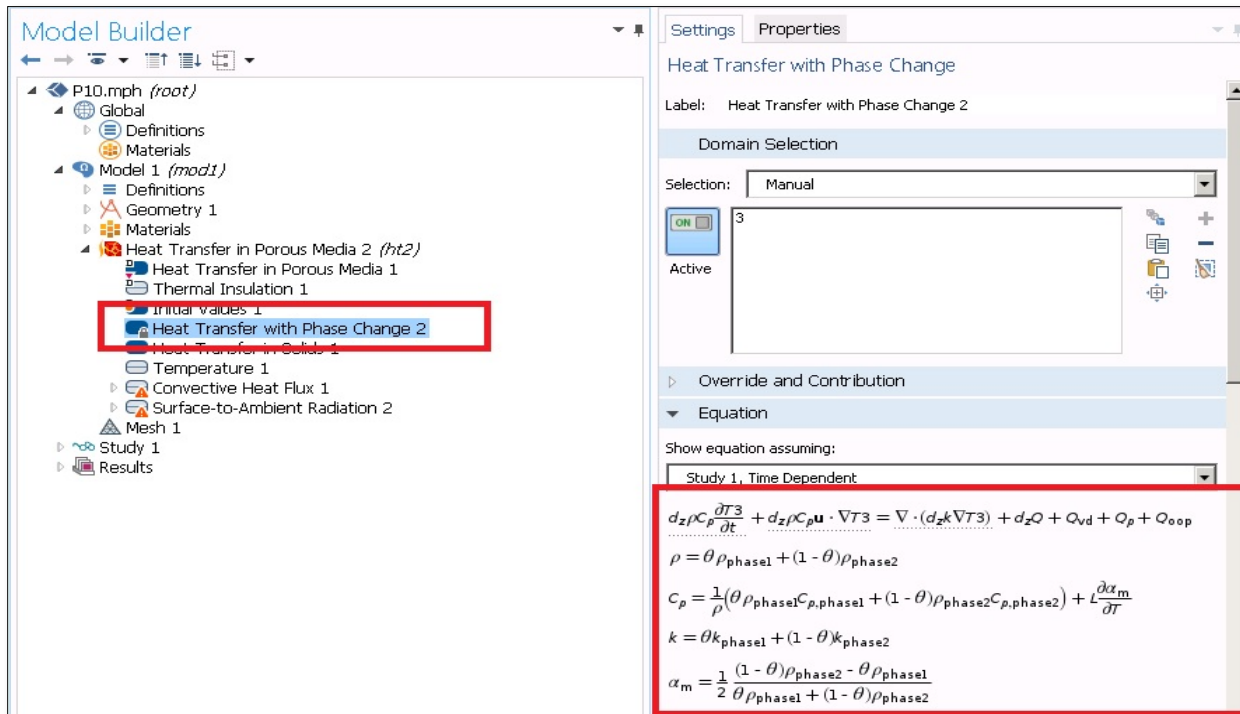


θ_m : Volume fraction of mortar

$(1 - \theta_m)$: Volume fraction of the porosity (the volume fraction filled with PCM)

$$\lambda_{eff} = \lambda_m \theta_m + \lambda_{PCM} (1 - \theta_m) \quad (\rho C_p)_{eff} = \rho_m C_{p,m} \theta_m + \rho_{PCM} C_{p,PCM} (1 - \theta_m)$$

Phase Change



β : Volume fraction of PCM at phase 1

$(1-\beta)$: Volume fraction of PCM at phase 2

$$\rho_{PCM} = \rho_{phase1} \beta + \rho_{phase2} (1 - \beta)$$

$$\lambda_{PCM} = \lambda_{phase1} \beta + \lambda_{phase2} (1 - \beta)$$

$$C_{p,PCM} = \frac{1}{\rho_{PCM}} (\rho_{phase1} C_{p,phase1} \beta + \rho_{phase2} C_{p,phase2} (1 - \beta)) + L \frac{\partial \alpha_m}{\partial T}$$

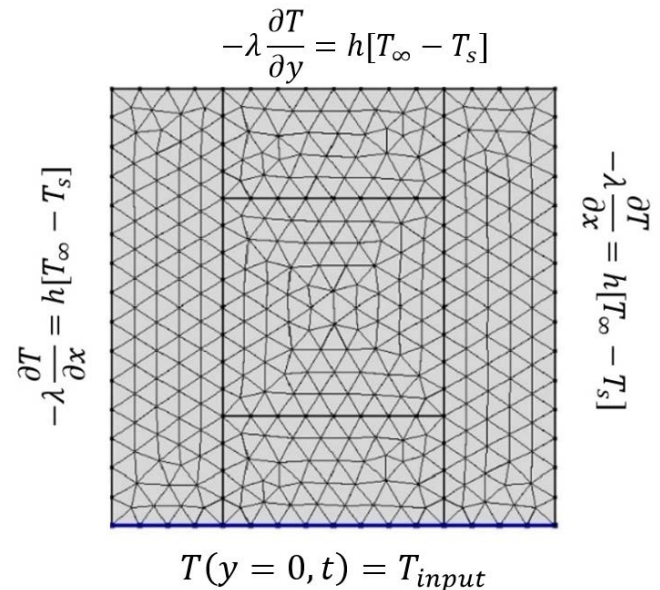
Conduction Heat Transfer:

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} = \frac{\rho C_p}{\lambda} \frac{\partial T}{\partial t}$$

Boundary Condition: $\left\{ \begin{array}{l} -\lambda \frac{\partial T}{\partial x} = h[T_\infty - T_s] \\ -\lambda \frac{\partial T}{\partial y} = h[T_\infty - T_s] \end{array} \right.$

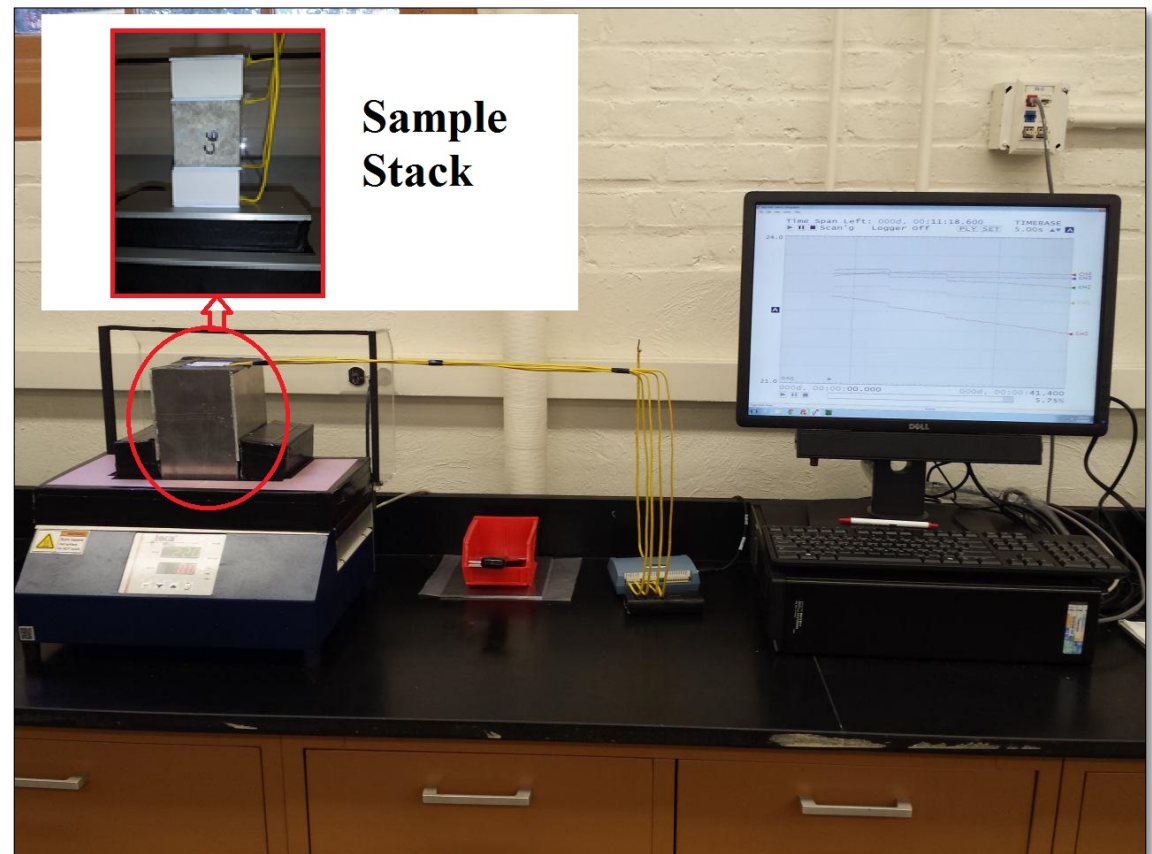
Initial Condition: $T(x, t = 0) = T_R$

Applying Temp.: $T(y = 0, t) = T_{input}$

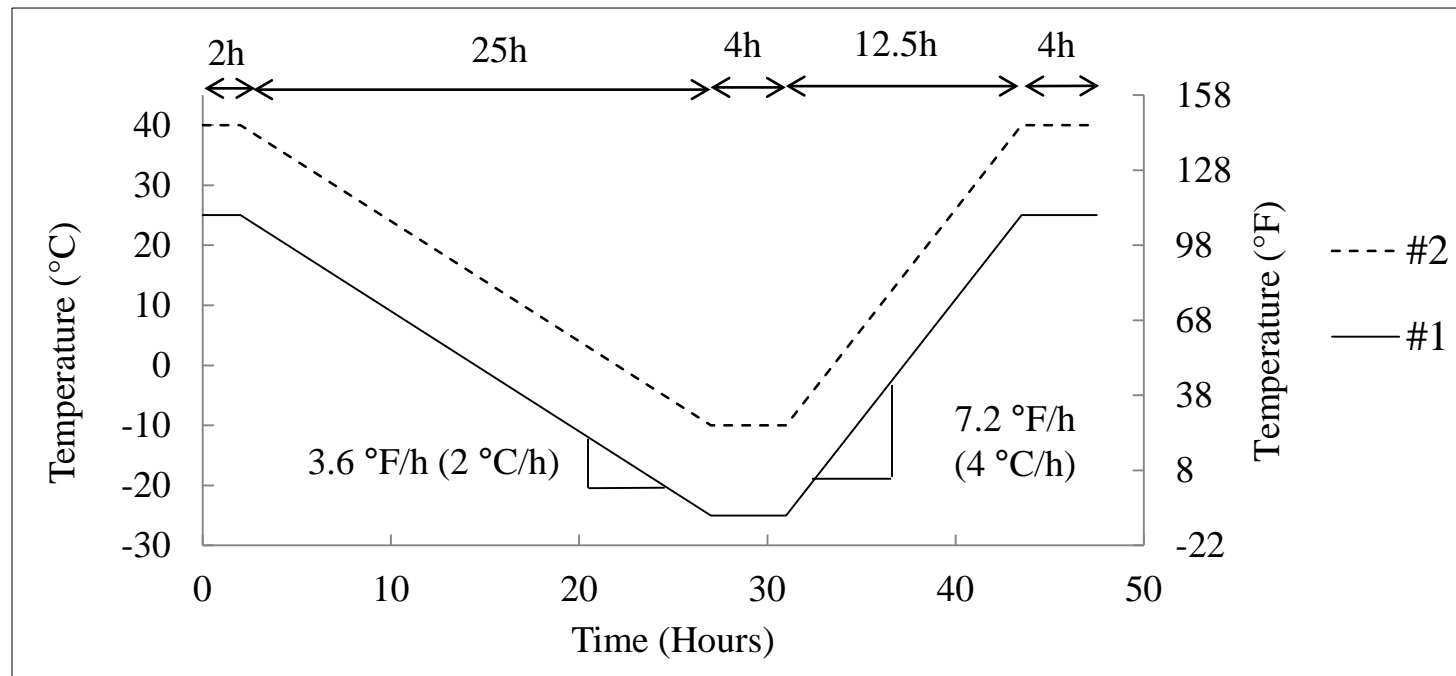


Guarded Longitudinal Calorimeter

- Cold Plate
- Sample Stack
- Insolation
- Thermocouples
- Data Acquisition
- Computer



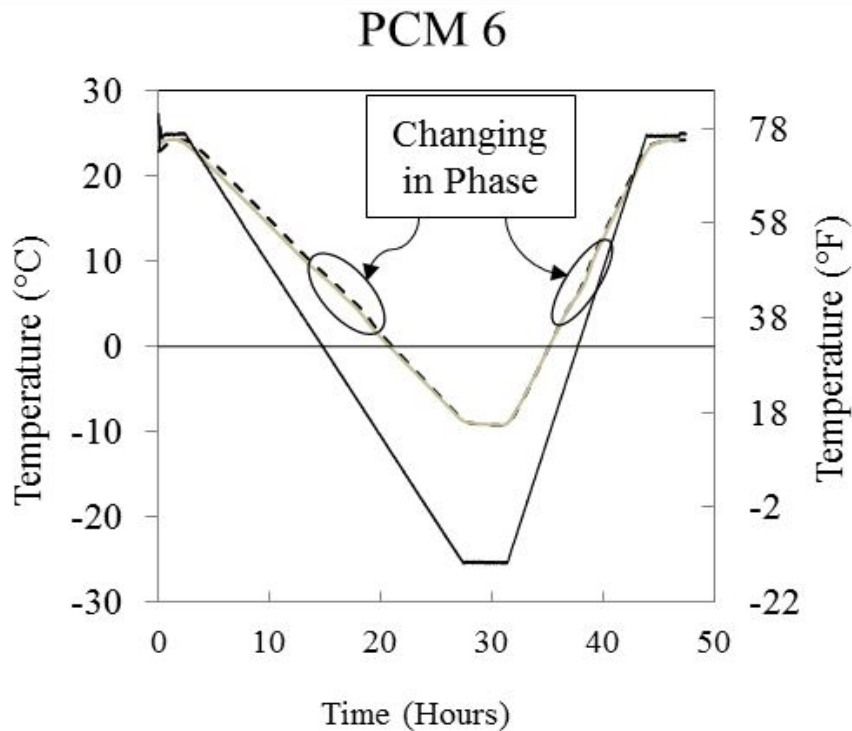
Applied Temperature Profiles



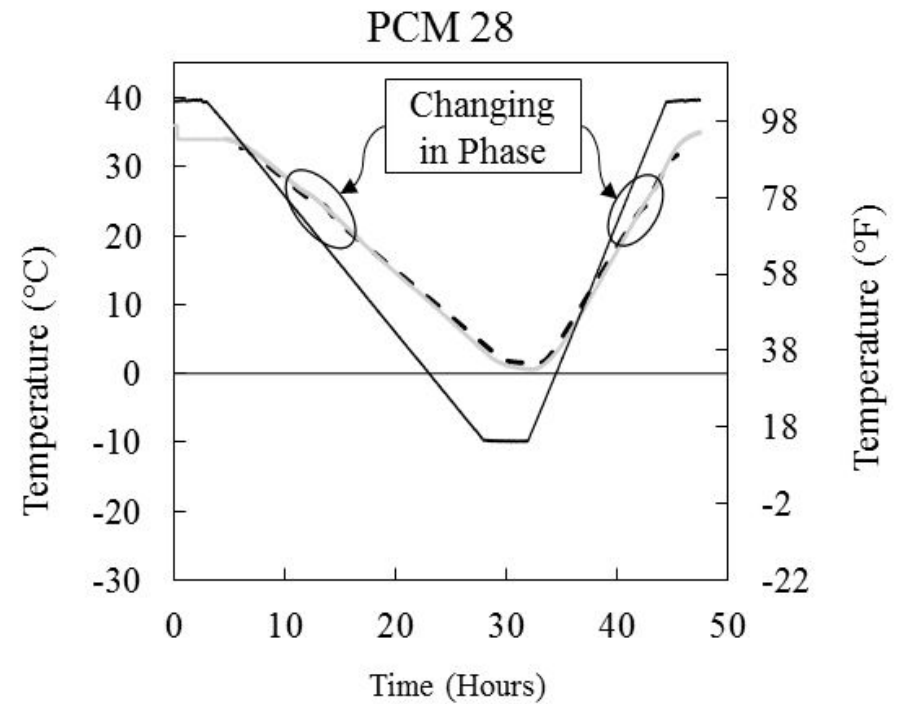
Number 1 for sample with PCM 6

Number 2 for sample with PCM 28

Comparing COMSOL simulation and laboratory experiment



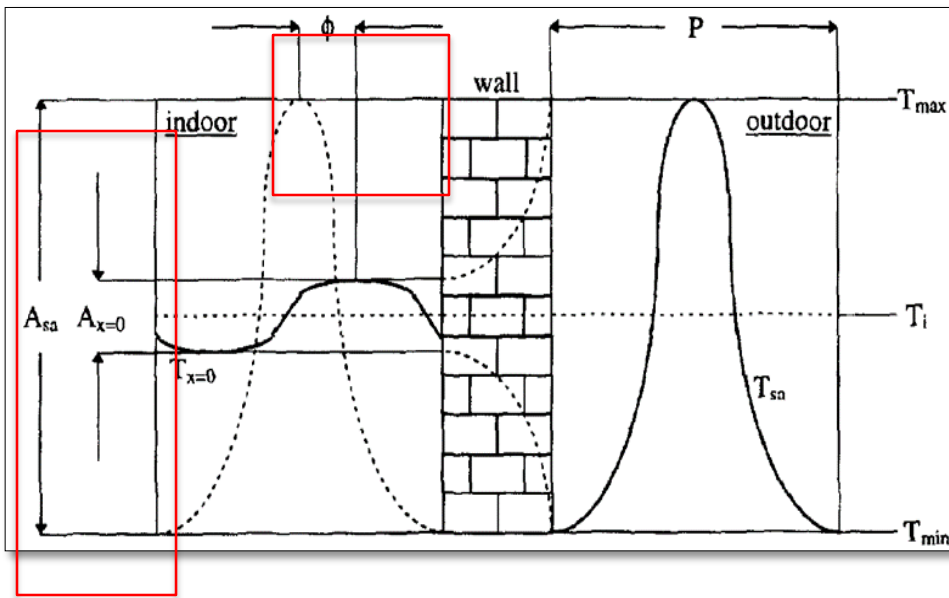
--- Top of the specimen-COMSOL Modeling
 — Top of the specimen-Laboratory Setup



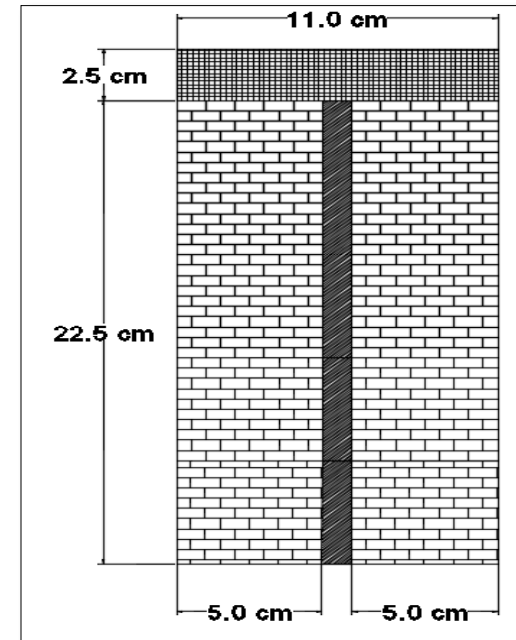
--- Top of the Specimen-COMSOL Modeling
 — Top of the Specimen-Laboratory Setup

Effect of different PCM percentages on the:

- 1) Time Lag
- 2) Decrement Factor (f)



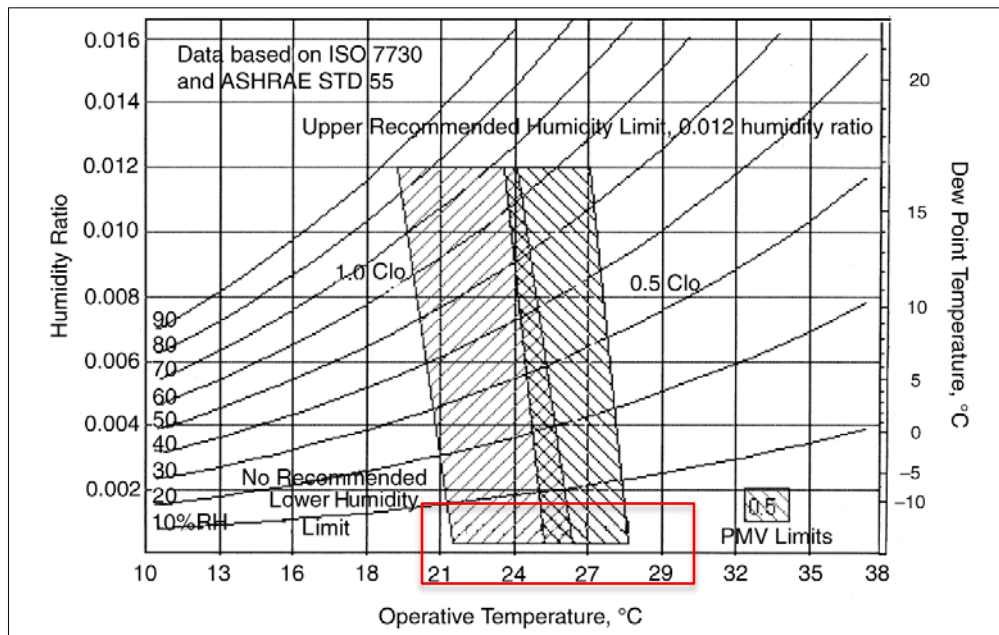
$$f = \frac{A_{x=0}}{A_{sa}}$$



Wall Cross Section

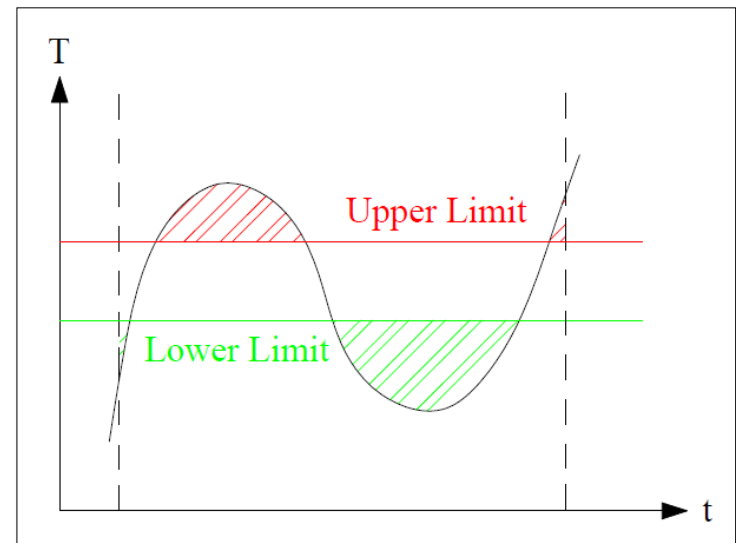
3) Duration of being in comfort zone

4) Energy required by HVAC



Comfort Zone:

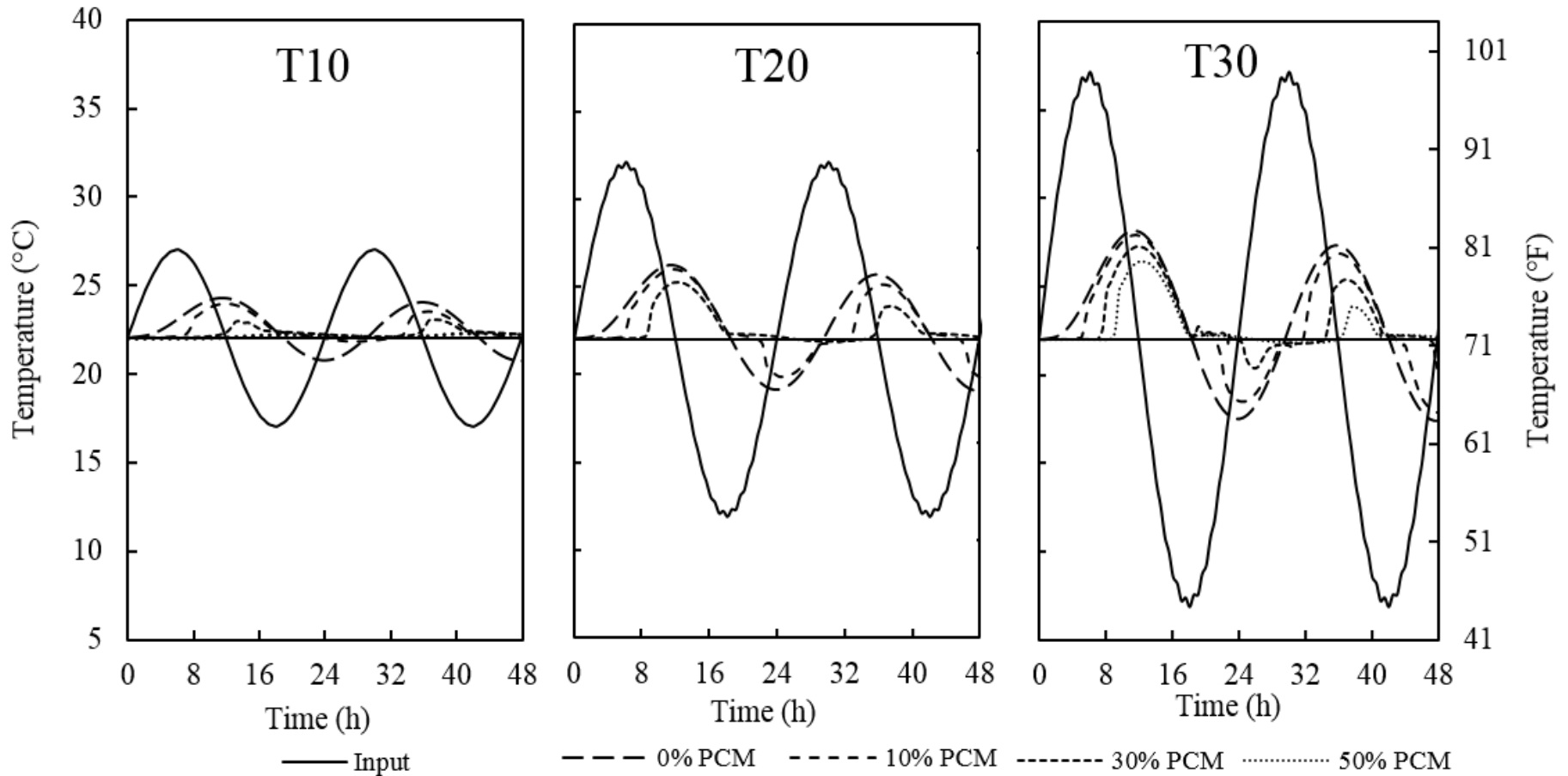
22 °C to 26 °C (71.6 °F to 78.8 °F)



$$\frac{dQ}{dt} = hA(T_R - T_S) \rightarrow$$

$$Q = hA \int_{t_1}^{t_2} (T_R - T_S) dt$$

Sine Functions



Comfort duration and the area out of the comfort zone for Sine functions

Input	PCM %	Percentage increase in the comfort time duration		Percentage decrease in the area out of comfort zone	
		22 ± 1.5 °C	22 ± 3.0 °C	22 ± 1.5 °C	22 ± 3.0 °C
T10	10	29	0	82	100
	30	41	0	100	100
	50	41	0	100	100
T20	10	69	18	43	63
	30	181	29	88	95
	50	202	33	98	100
T30	10	75	26	26	35
	30	208	97	73	84
	50	323	118	92	93

Real Temperature Changes of Different Cities

City	Time	PCM %	Percentage increase in the comfort time duration	Percentage decrease in the area out of comfort zone
Seattle, Washington	Second week Aug. 1996	10	8	16
		30	18	27
		50	32	39
San Diego, California	Second week Sep. 2004	10	4	9
		30	31	29
		50	38	42
San Antonio, Texas	Second week Aug. 1990	10	1	5
		30	2	7
		50	4	10
Miami, Florida	Third week May 2000	10	2	6
		30	3	8
		50	5	12
Minot, North Dakota	Second week Jun. 1980	10	8	17
		30	23	39
		50	28	43
Denver, Colorado	Second week Jul. 2004	10	15	28
		30	24	39
		50	27	48

- COMSOL Multiphysics® software can accurately simulate changes in temperature in porous media, such as gypsum boards, and can accurately take the effects of phase transition of PCMs into account.
- Under sine function inputs, depending on the percentage of the PCM, the inside peak temperature can be delayed by up to 7 hours and be decremented by up to 80%.
- For the real changes in temperature of different cities, the comfort duration was increased by up to 40% and almost half of the energy required by HVAC systems was reduced.
- **Future Works:**

More studies should be conducted to find the optimum percentage and melting temperature of PCM for different cities. Furthermore, cost analysis should also be conducted to compare the efficiency of PCMs to alternative methods.

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- 14. Sharifi, N.P., G.E. Freeman, and A.R. Sakulich, Using COMSOL Modeling to Investigate the Efficiency of PCMs to Modify the Temperature Changes in Cementitious Materials, Case Study, Submitted to *Construction and Building Materials* (2015)
- 15. Asan, H. and Y. Sancaktar, Effects of wall's thermophysical properties on time lag and decrement factor, *Energy and Buildings*, **28**(2), 159-166 (1998)
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THANKS FOR YOUR
ATTENTION!



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