

COMSOL Multiphysics application in modeling PEMFC transients

Li Xiaojin (Associate Professor)



Dalian Institute of Chemical Physics, Chinese Academy of
Science

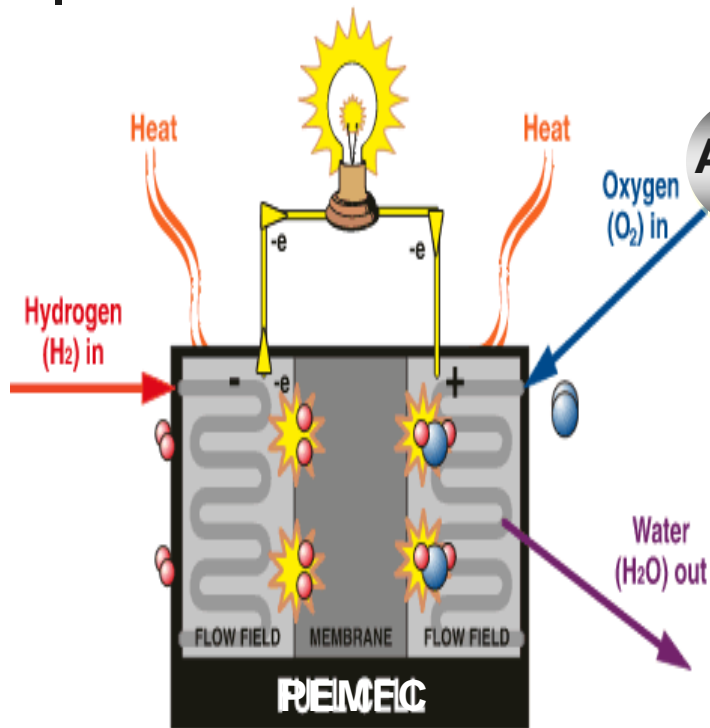
Shanghai 26th, October, 2010



Main content

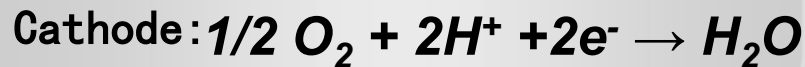
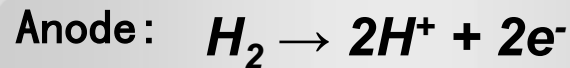
- Principle of PEMFC and transient characteristics
- Study on PEMFC transient characteristics
 - Develop the PEMFC transient model
 - Air stoichiometry change on PEMFC transient
 - Water transport on PEMFC transient
 - Modeling high temperature PEMFC
- Conclusion

Principle of PEMFC & application

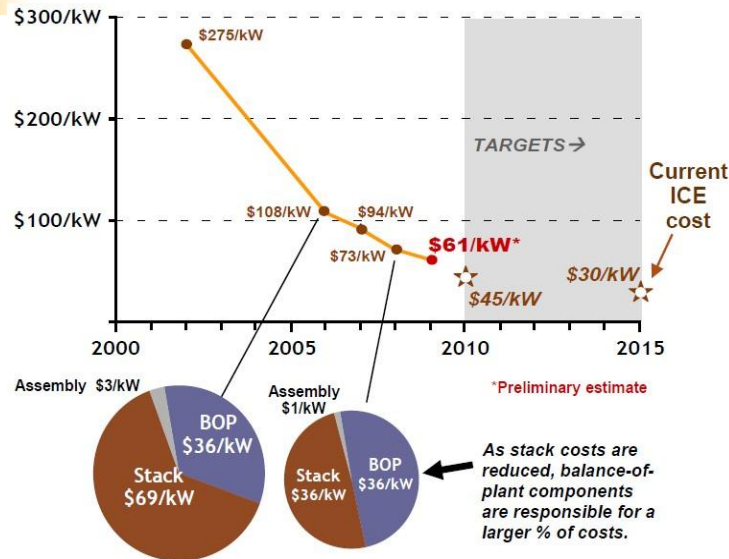


Advantages

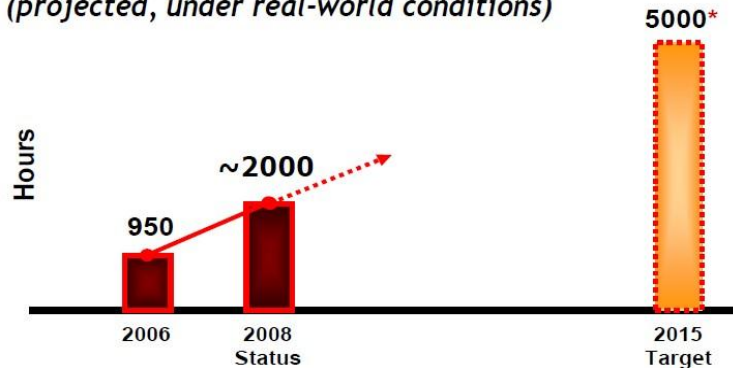
- High efficiency
- Environment friendly
- High power density
- Fast startup



Bottleneck of FC technology



Transportation Fuel Cell System Durability
(projected, under real-world conditions)



* 5000 hours corresponds to roughly 150,000 miles of driving

Commercialization

- System stability & reliability

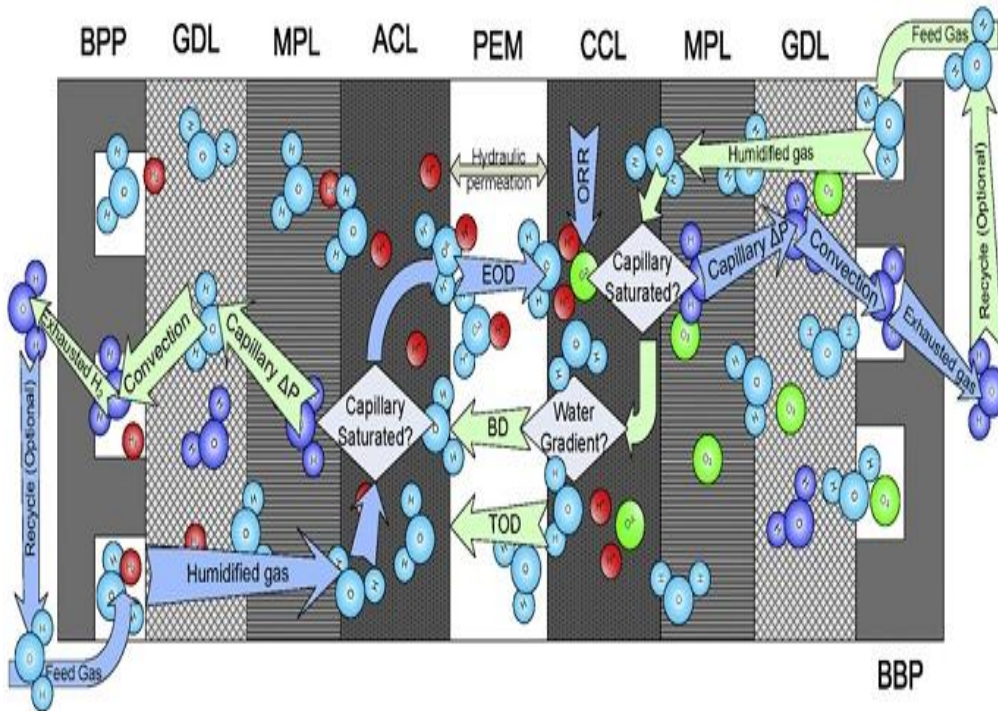
Transient characteristics

- System cost

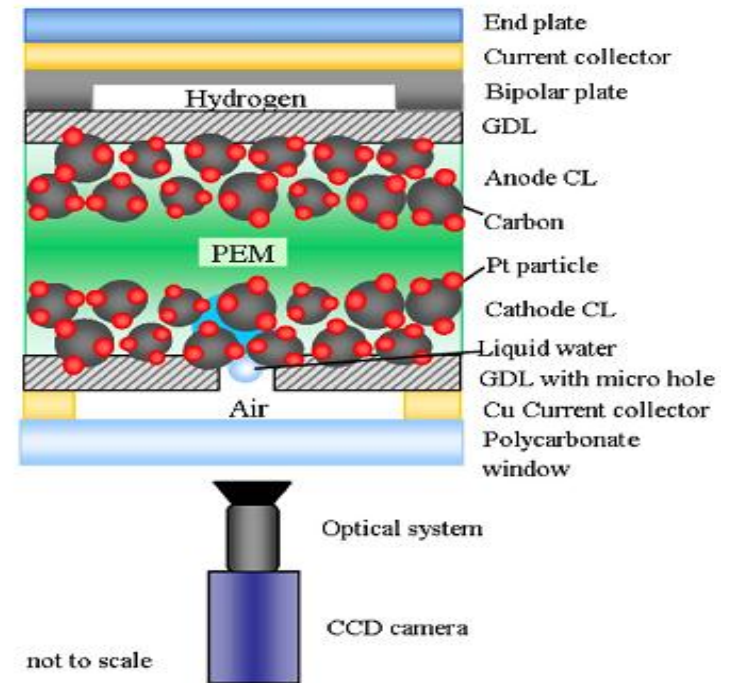
- Environment adaptability

Water transport in FC

FC water transport principle



Experiment observation





Model assumptions

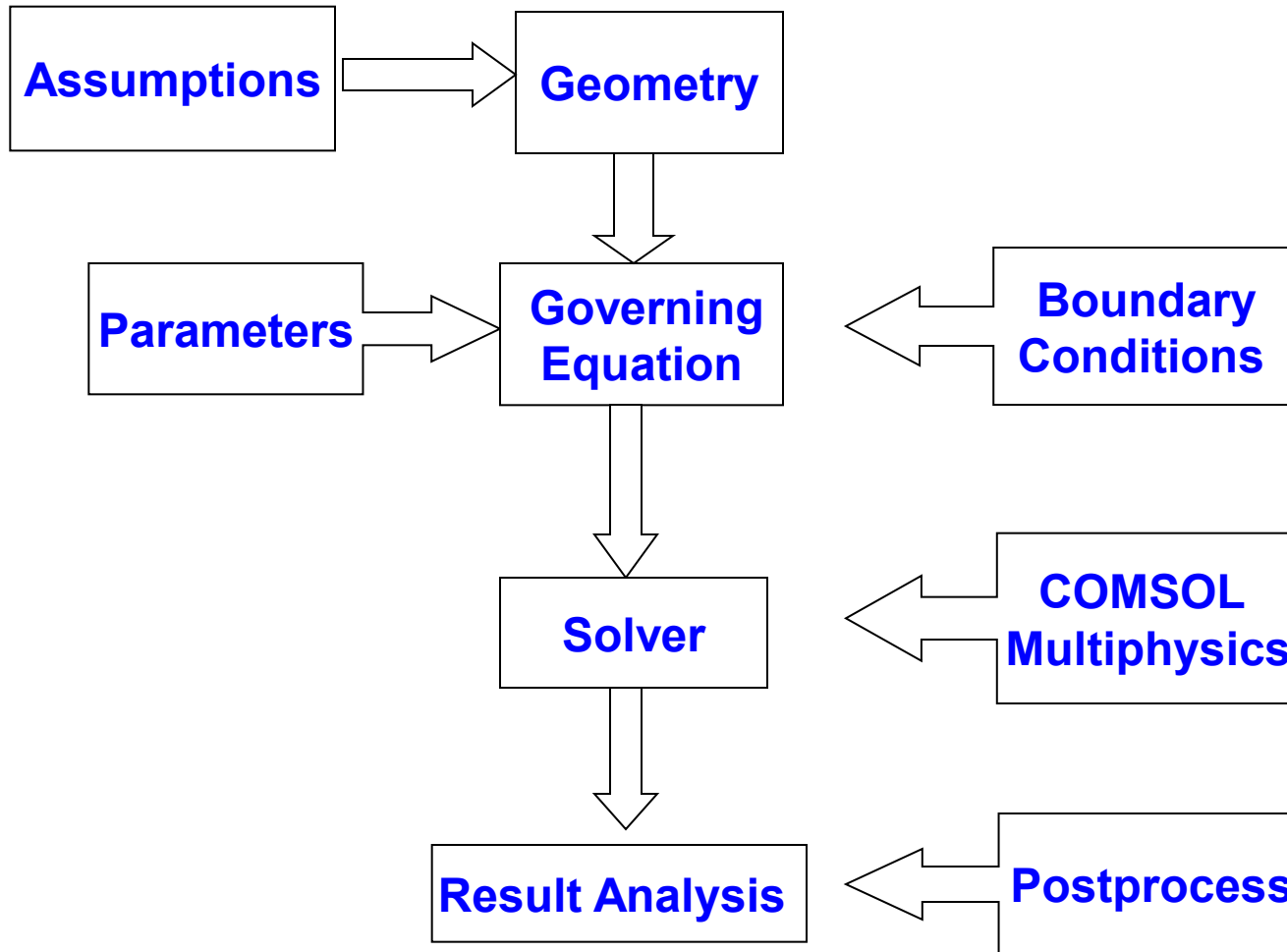
1. The gravity effect is neglected ;
2. The gas mixture is an incompressible ideal gas ;
3. The flow in the gas channel is laminar ;
4. The diffusion layer, catalyst layer and membrane are isotropic and homogeneous, and the membrane is impermeable to gas species ;
5. The contact resistance between any two parts in the fuel cell is neglected ;
6. The dissolved reactive gas in electrolyte phase of catalyst layer is neglected ;
7. It is considered that water exits in the gas phase at the electrodes as well as in the liquid phase within the membrane. In channels, existence of liquid water is in a small volume fraction and in finely dispersed droplets so that it does not affect the gas flow.



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Procedures





Model equations

Continuity: $\nabla \cdot (\rho u) = S_m$

Momentum: $\frac{1}{\varepsilon^2} \nabla \cdot (\rho \vec{u} \vec{u}) = -\nabla p + \nabla \cdot \tau + S_u$

Species: $\nabla \cdot (-D_i^{eff} \nabla C_v) + \nabla \cdot (u_g C_i) = S_i$

Water in membrane: $\nabla \cdot \left(\frac{n_d I}{F} - D_w \nabla c_w \right) = 0$

Energy: $\rho c_p u \cdot \nabla T + \nabla \cdot (-k_f \nabla T) = S_T$

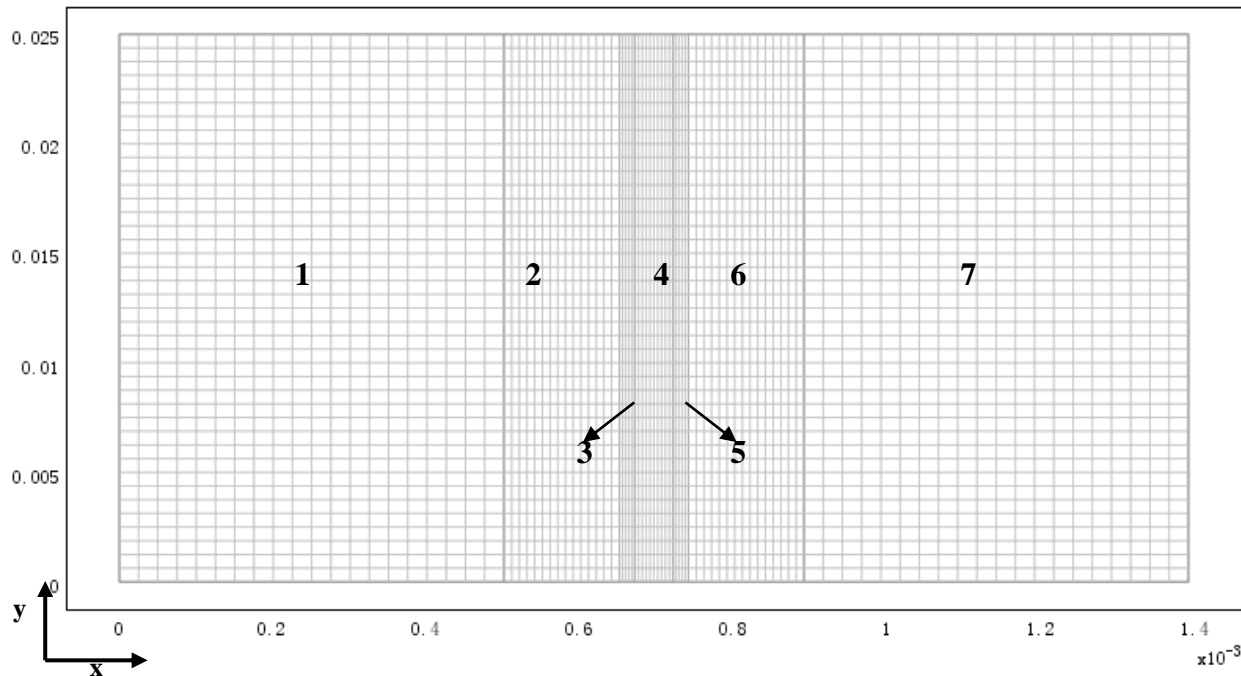
Electron: $\nabla \cdot (-\sigma_e^{eff} \nabla \Phi_e) = S_e$

Proton: $\nabla \cdot (-\sigma_m^{eff} \nabla \Phi_m) = -S_m$

Source term for model equations

	GDL	CL, a	CL, c	Membrane
Mass	/	$S_m = M_{H_2} S_{H_2} + M_{H_2O} S_w^a$	$S_m = M_{H_2O} S_{O_2} + M_{H_2O} S_w^c$	/
Momentum	$S_u = -\frac{\mu}{k_p} u$	$S_u = -\frac{\mu}{k_p} u$	$S_u = -\frac{\mu}{k_p} u$	/
Species	/	$S_{H_2} = -\frac{i_a}{2F}$	/	/
	/	/	$S_{O_2} = -\frac{i_c}{4F}$	/
	/	$S_w^a = -\frac{n_d}{F} i_a$	$S_w^c = \frac{n_d}{F} i_c + \frac{i_c}{2F}$	/
Electron	/	$S_s = -i_a$	$S_s = i_c$	/
Proton	/	$S_e = i_a$	$S_e = -i_c$	/
Energy	$S_T = \frac{i^2}{\sigma_c}$	/	$S_{rm} = -j(\Phi_e - \Phi_s - \frac{T\Delta S}{nF})$	$S_T = \frac{i^2}{\sigma_m}$

Model geometry & mesh



Model geometry: 1 anode flow channel, 2 anode gas diffusion layer, 3 anode catalyst layer, 4 membrane, 5 Cathode catalyst layer, 6 Cathode gas diffusion layer, 7 Cathode flow channel

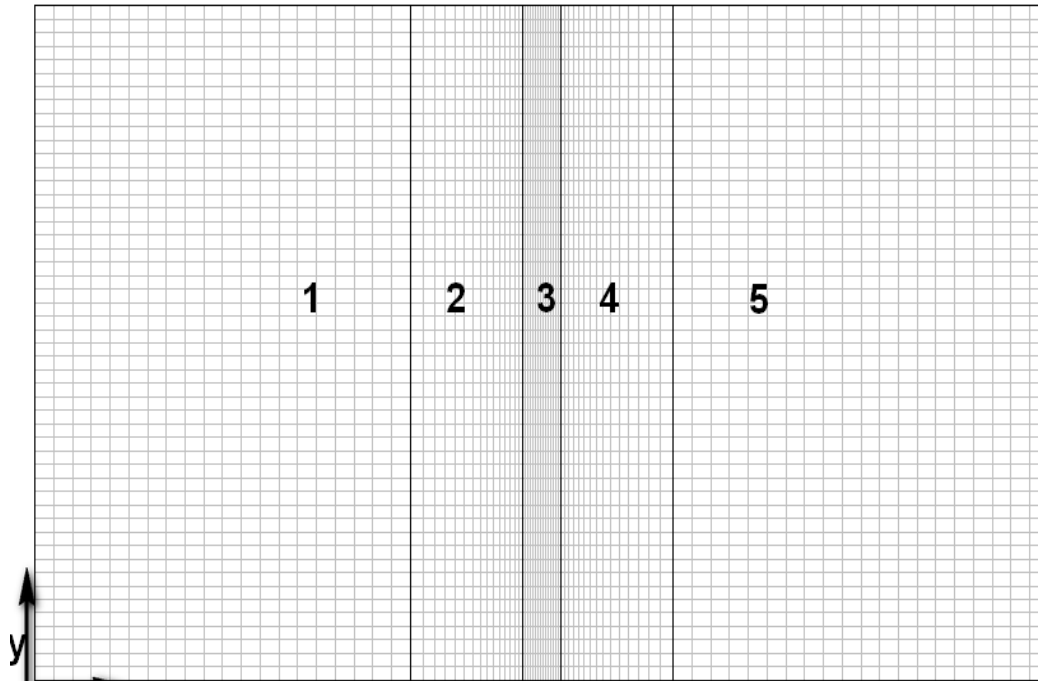
Comsol Multiphysics 3.5



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PEMFC transient model



Model geometry: 1 anode flow channel,
2 anode gas diffusion layer, 3 membrane,
4 Cathode gas diffusion layer, 5 Cathode
flow channel

Mass conservation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{u}) = S_m$$

Momentum conservation

$$\frac{1}{\varepsilon} \left[\frac{\partial \rho \vec{u}}{\partial t} + \frac{1}{\varepsilon} \nabla \cdot (\rho \vec{u} \vec{u}) \right] = -\nabla p + \nabla \cdot \tau + S_u$$

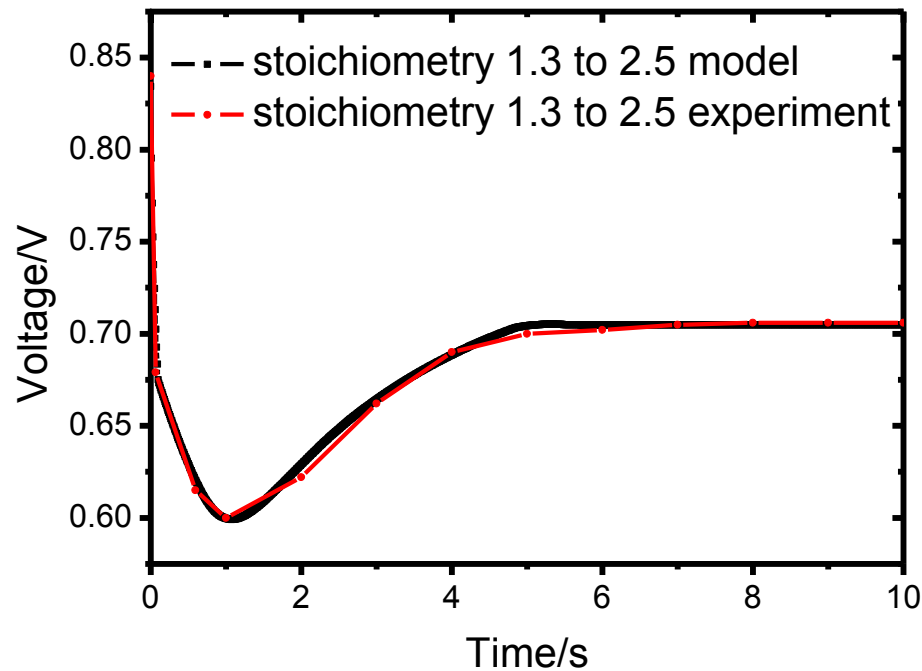
Species conservation

$$\frac{\partial c_k}{\partial t} + \nabla \cdot (\vec{u} c_k) = \nabla \cdot (D_k^{eff} \nabla c_k) + S_k$$

Cell potential:

$$V_{cell} = E - \eta_{act} - \eta_{ohm} - \eta_{conc}$$

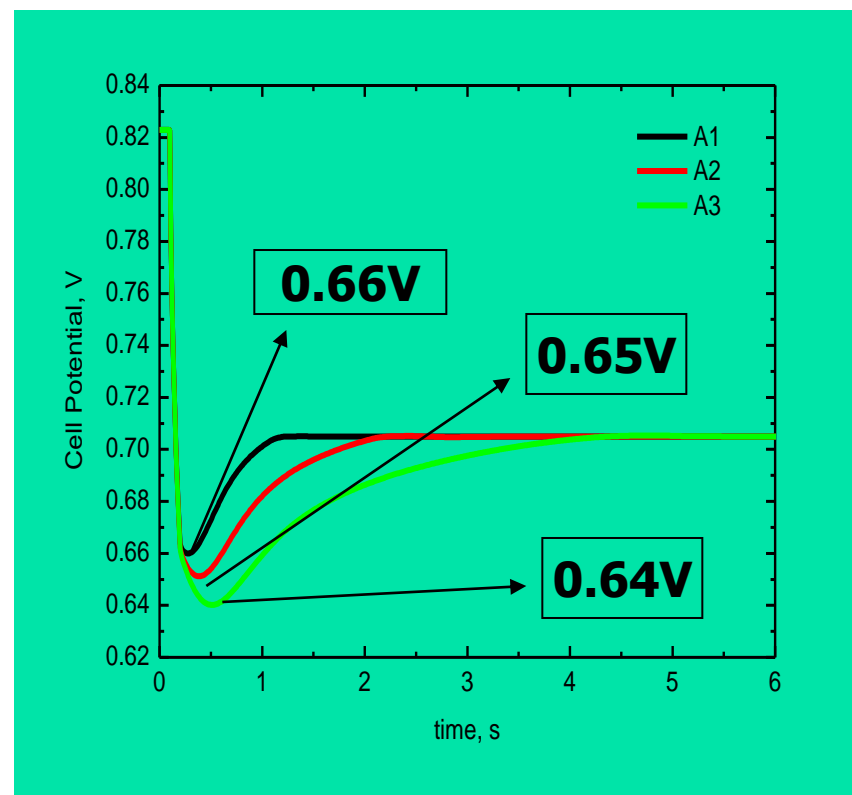
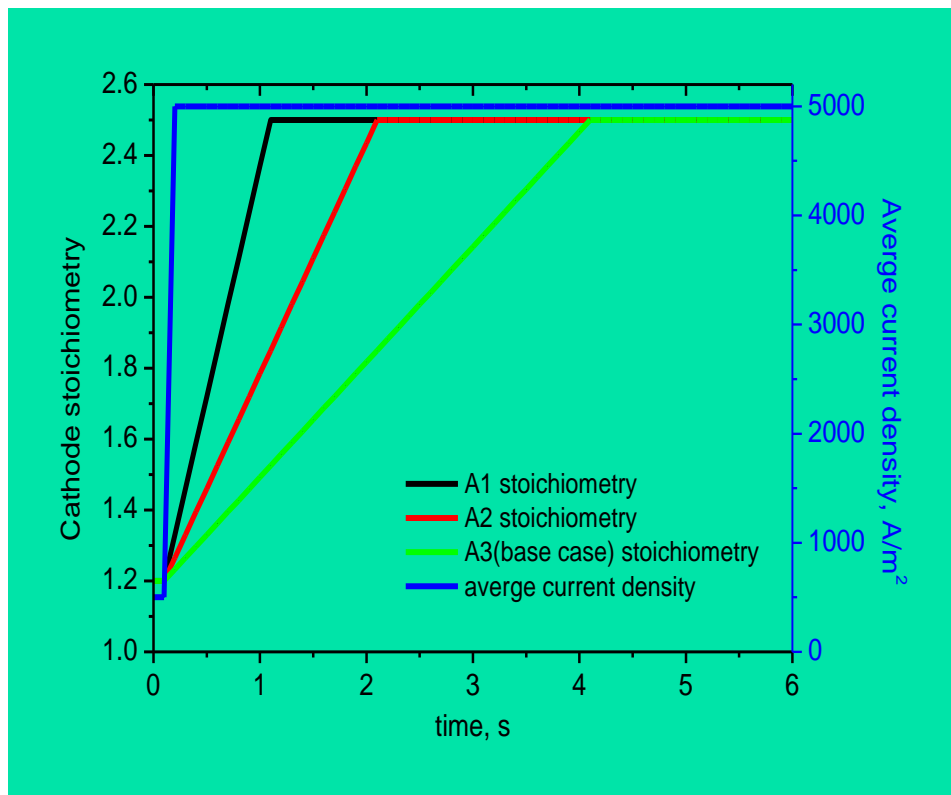
Model validation



Comparison between model and experimental cell voltage evolution

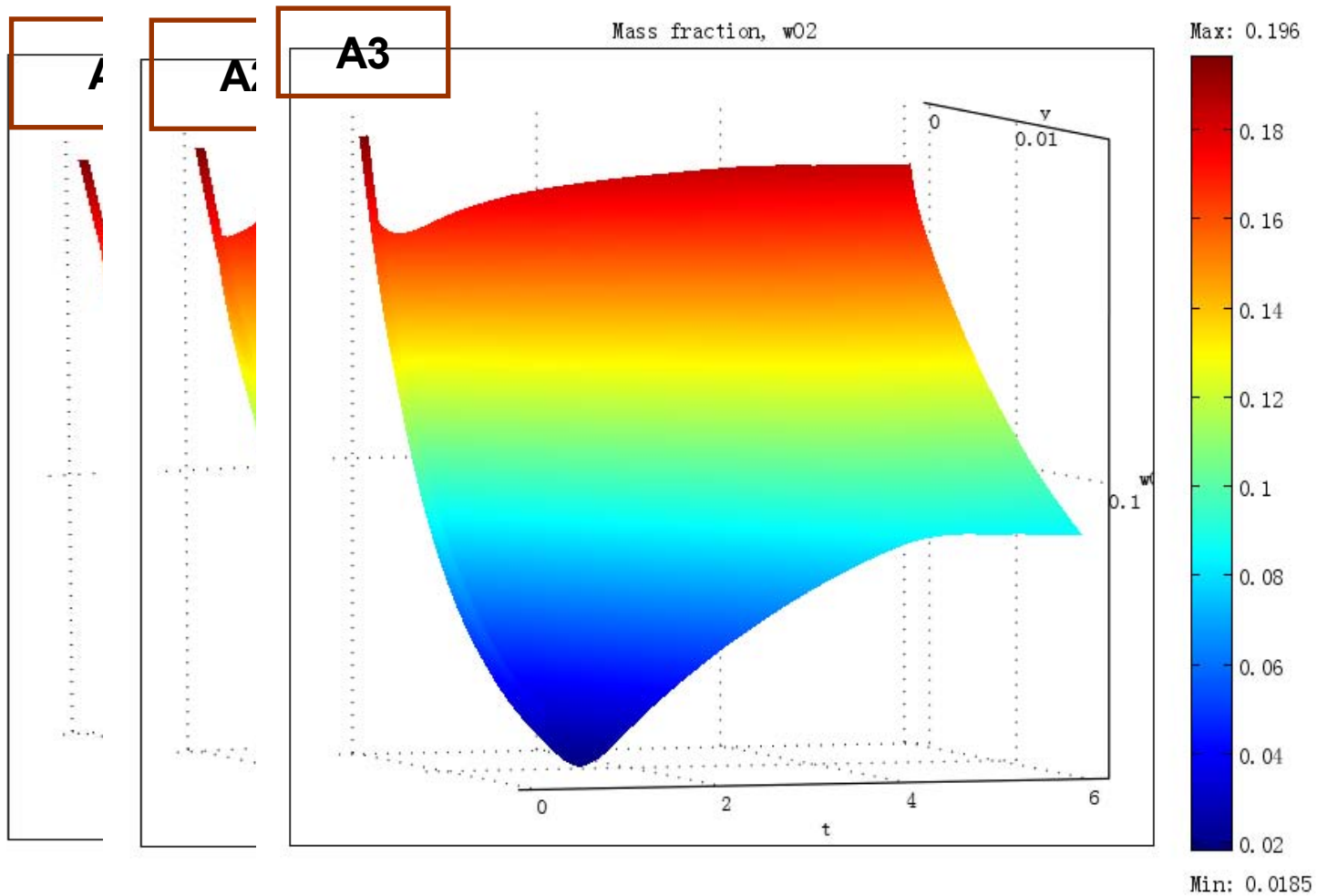
Q. Shen, M. Hou, et. al J. Power Sources. 2008, 179: 292–296

Air stoichiometry change on PEMFC transient



Qu Shuguo, Li Xiaojin, etc., J Power Sources 185 (2008), 302-310

Reactant starvation under different conditions





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Experiment study on water dynamic transport

Aim: Study water transport in fuel cell under different humidity on cell potential and as model validation

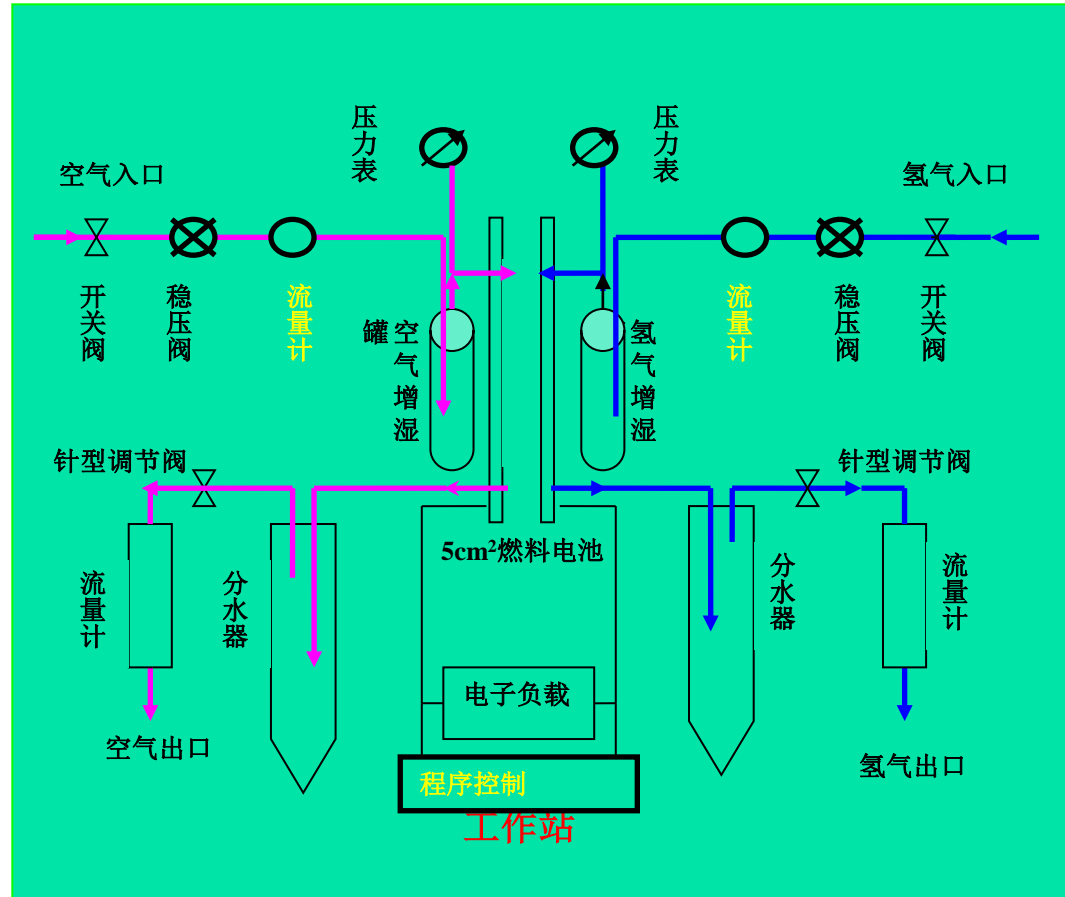
Conditions:

Current: step from 0.05 to 2.5A

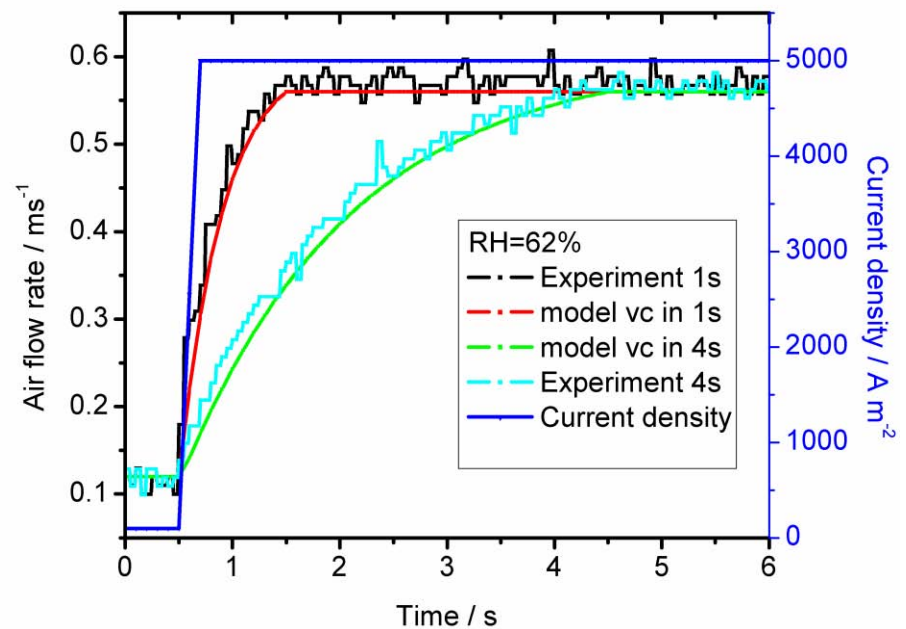
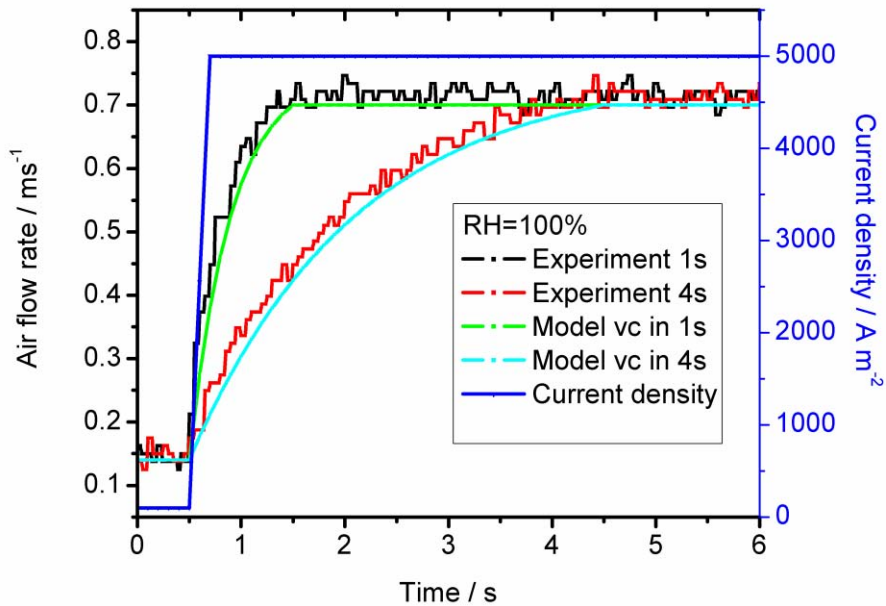
Air flow: parabolic pattern
22-110ml/min

Hydrogen flow: fixed

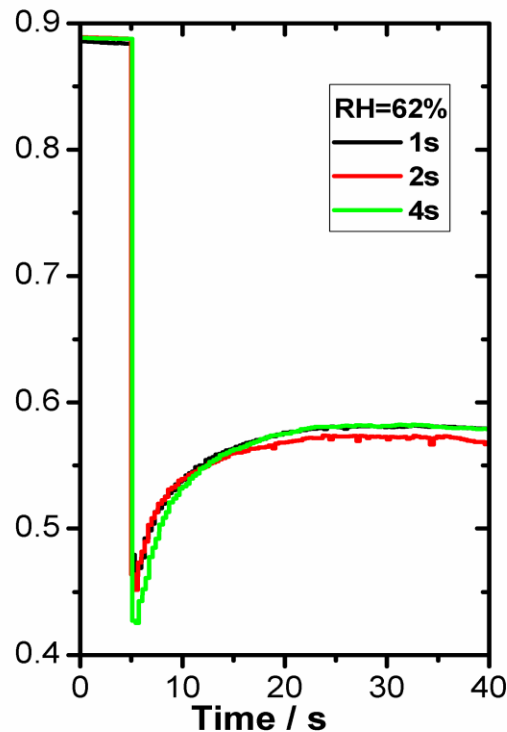
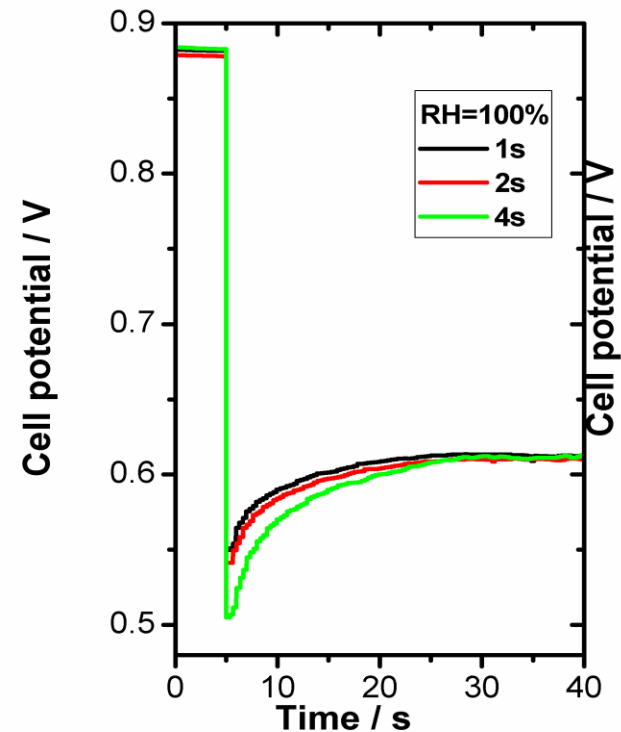
Humidity: 100%
62%



Average current density & cathode inlet velocity change

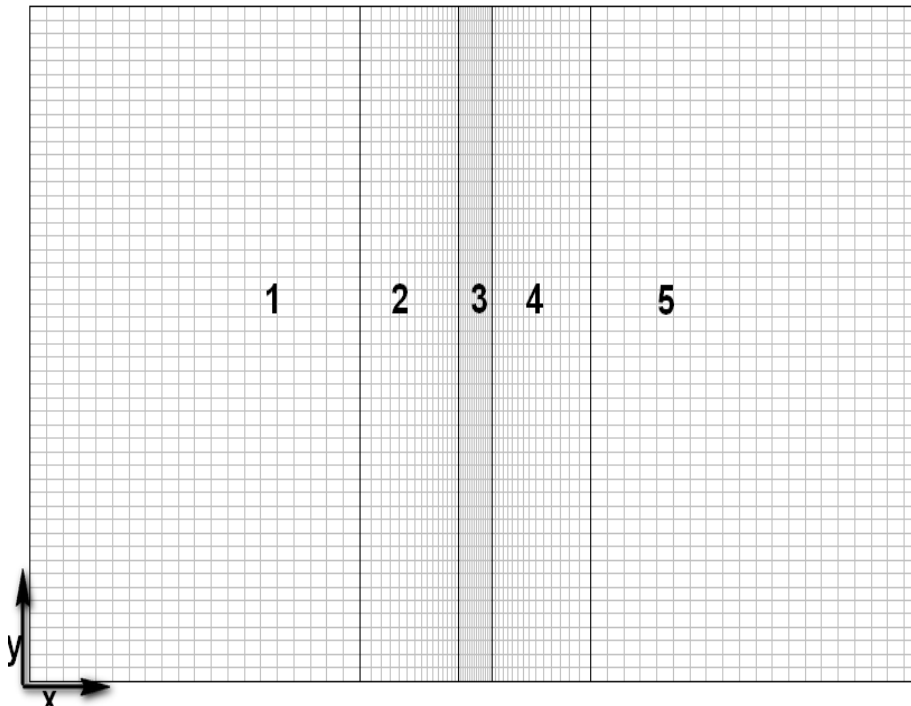


Experiment results



- ✓ For same relative humidity, the lower the change rate, the greater the cell potential undershoots.
- ✓ For different relative humidity, the magnitude of cell potential undershoots increased as the relative humidity decreased
- ✓ The steady state cell potential also decreased as the relative humidity was decreasing

Model geometry



Model geometry: 1 anode flow channel,
2 anode gas diffusion layer, 3 membrane,
4 Cathode gas diffusion layer, 5 Cathode
flow channel

Continuity
$$\frac{\partial}{\partial t}(\varepsilon \rho_g) + \nabla \cdot (\rho_g \vec{u}_g) = S_m$$

Momentum
$$\frac{1}{\varepsilon} \left[\frac{\partial \rho \vec{u}}{\partial t} + \frac{1}{\varepsilon} \nabla \cdot (\rho \vec{u} \vec{u}) \right] = -\nabla p + \nabla \cdot \tau + S_u$$

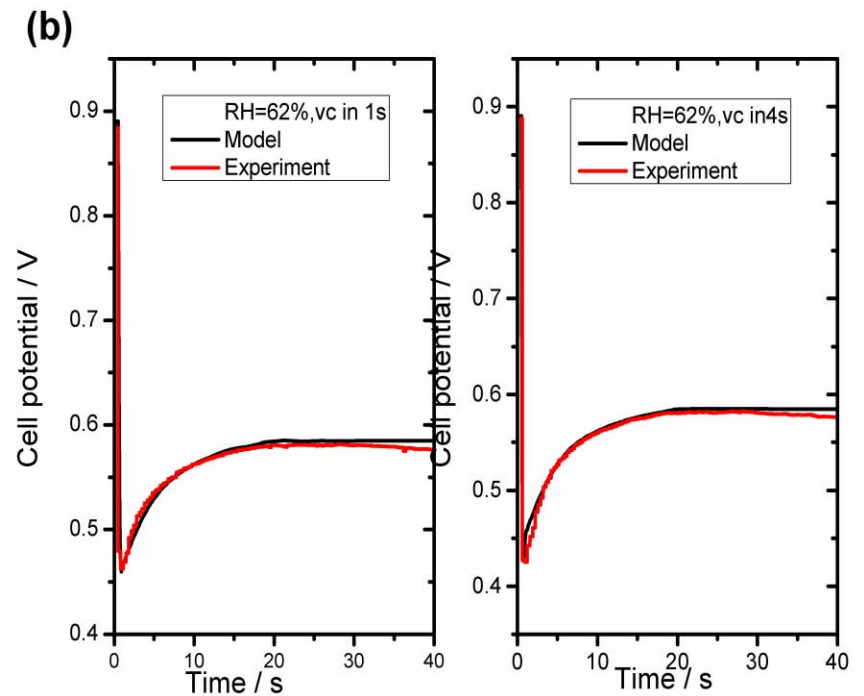
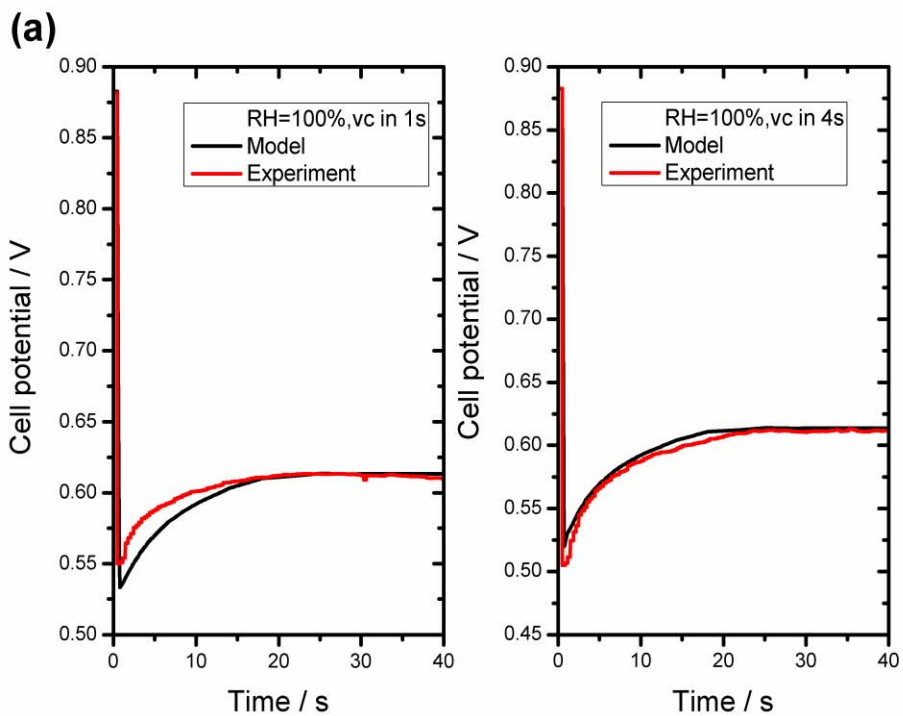
Species
$$\frac{\partial}{\partial t}(\varepsilon^{eff} C_i) + \nabla \cdot (-D_i^{eff} \nabla C_i) + \nabla \cdot (u_g C_i) = S_i$$

Water in membrane
$$\varepsilon_m \frac{\partial c_w}{\partial t} + \nabla \cdot \left(\frac{n_d I}{F} - D_w \nabla c_w \right) = 0$$

Electrons
$$\nabla \cdot (-\sigma_e^{eff} \nabla \Phi_e) = S_e$$

Protons
$$\nabla \cdot (-\sigma_m^{eff} \nabla \Phi_m) = -S_m$$

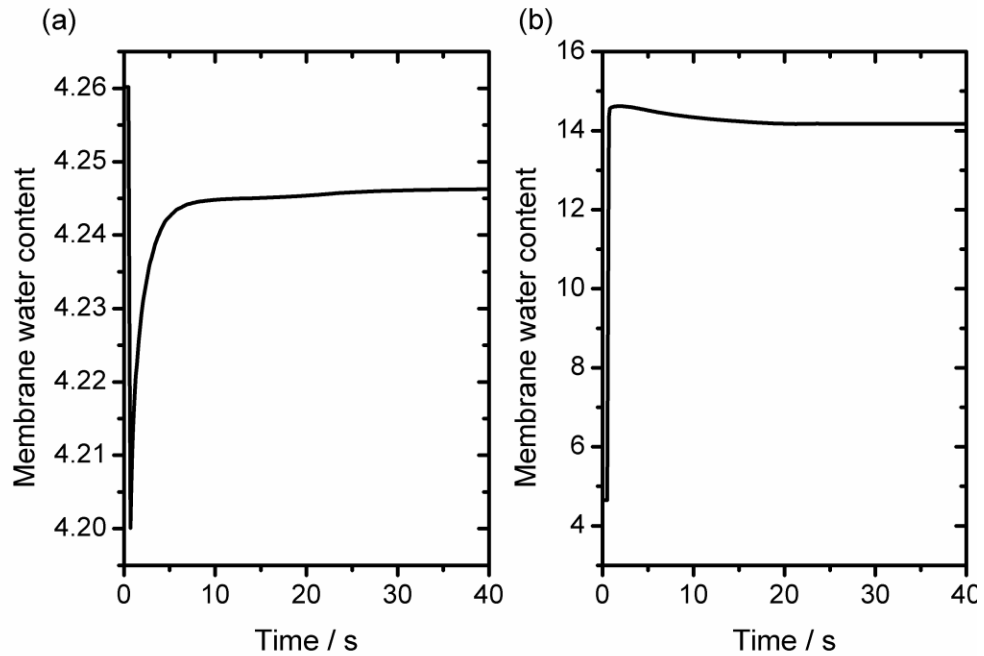
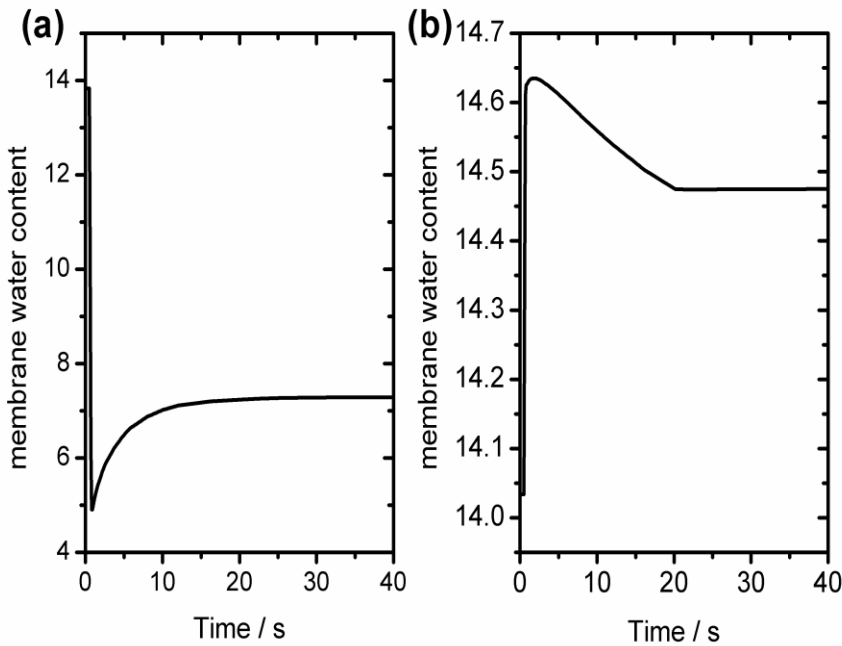
Model validation



Water content change at membrane/electrode interface

RH=100% water content at membrane/electrode interface

RH=62% water content at membrane/electrode interface



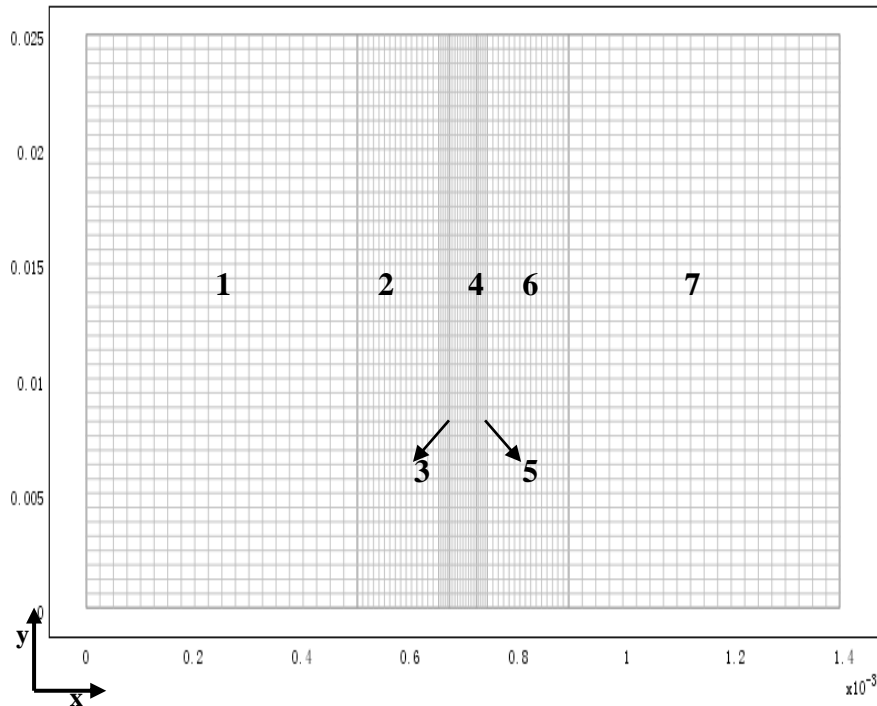
Qu Shuguo, Li Xiaojin, etc., J Power Sources 195 (2010), 6629-6636



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2-D nonisothermal HT-PEMFC model



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Continuity: $\nabla \cdot (\rho u) = S_m$

Momentum: $\frac{1}{\varepsilon^2} \nabla \cdot (\rho \vec{u} \vec{u}) = -\nabla p + \nabla \cdot \tau + S_u$

Species: $\nabla \cdot (-D_i^{eff} \nabla C_v) + \nabla \cdot (u_g C_i) = S_i$

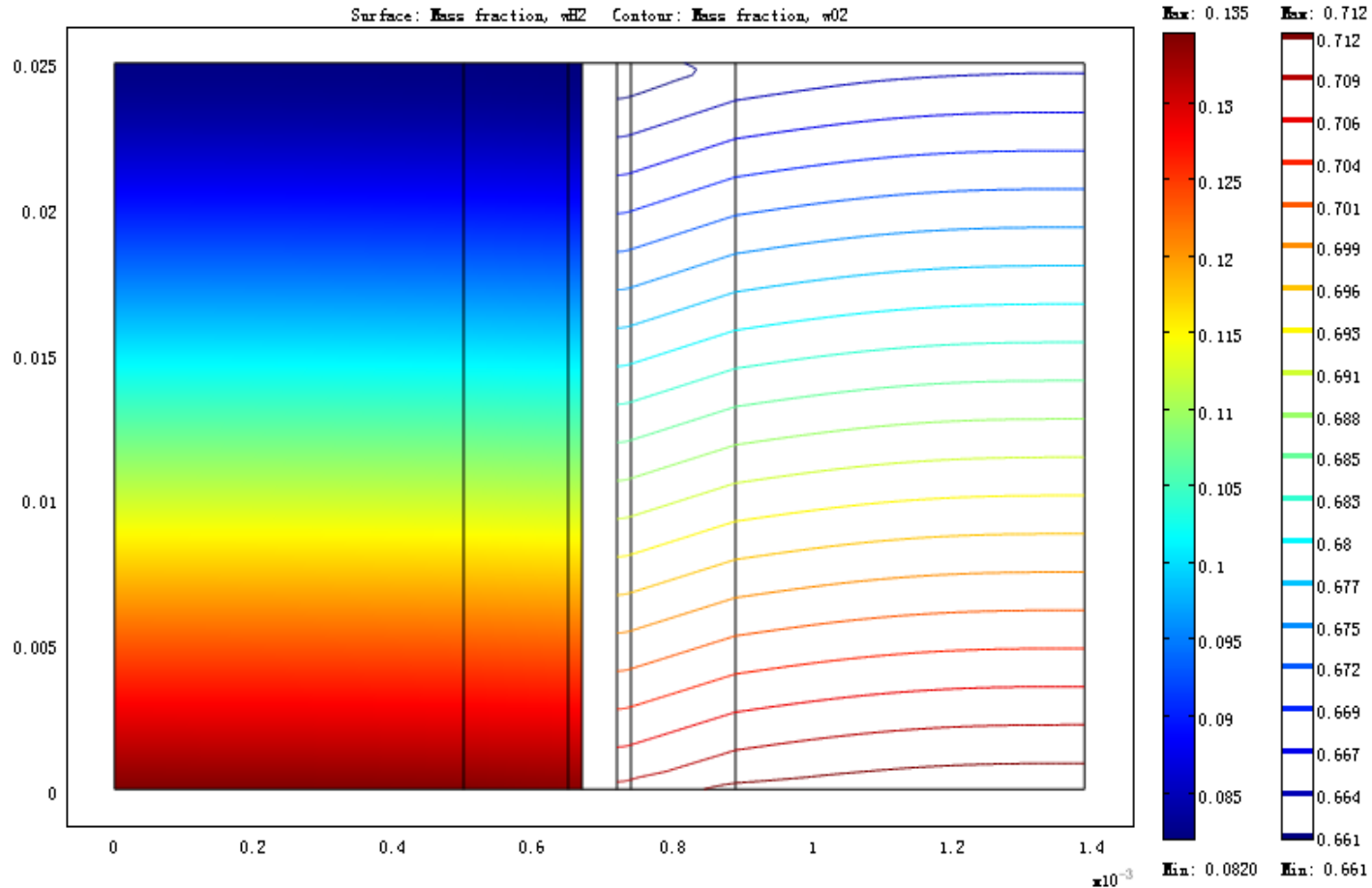
Water in membrane: $\nabla \cdot \left(\frac{n_d I}{F} - D_w \nabla c_w \right) = 0$

Energy: $\rho c_p u \cdot \nabla T + \nabla \cdot (-k_f \nabla T) = S_T$

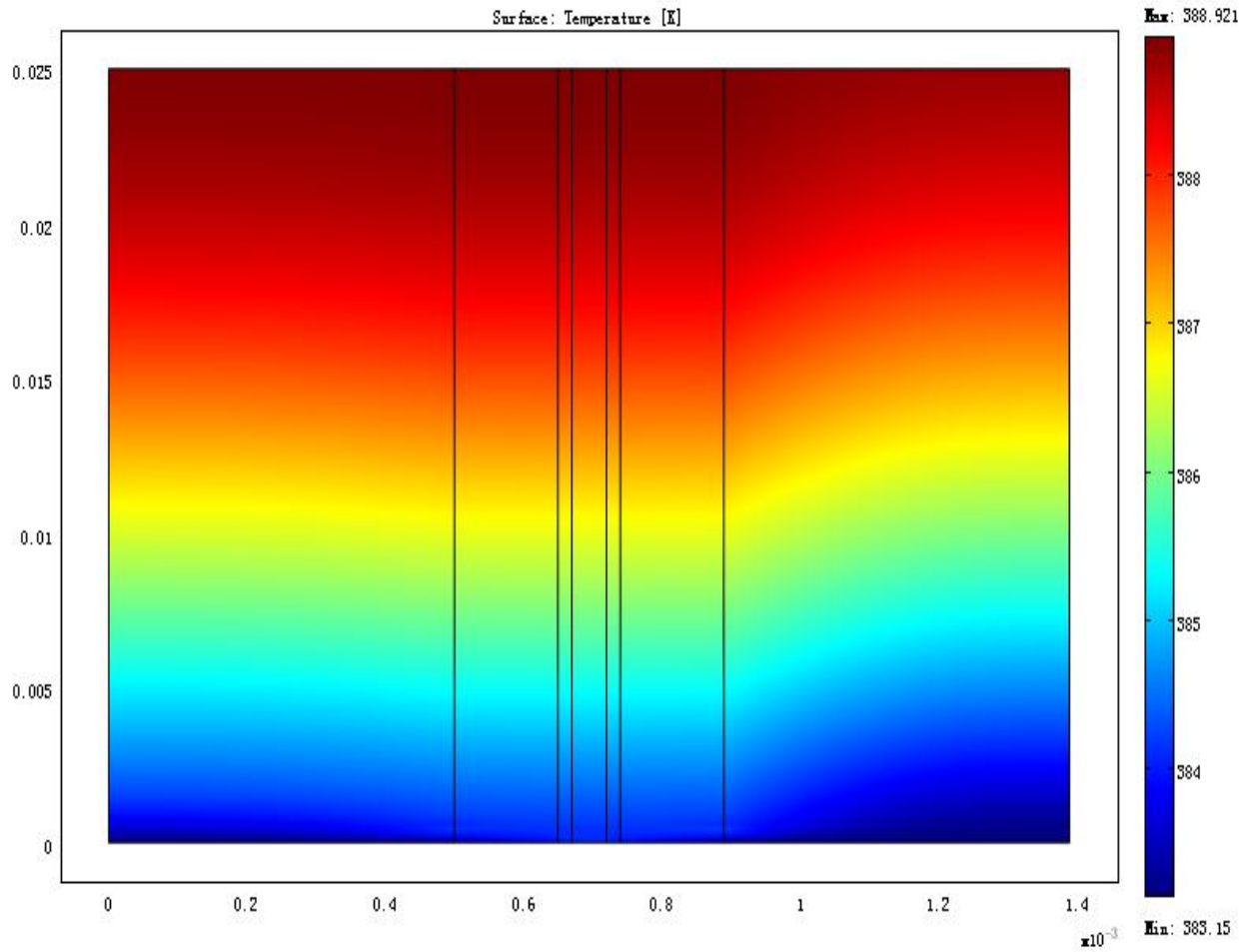
Electron: $\nabla \cdot (-\sigma_e^{eff} \nabla \Phi_e) = S_e$

Proton: $\nabla \cdot (-\sigma_m^{eff} \nabla \Phi_m) = -S_m$

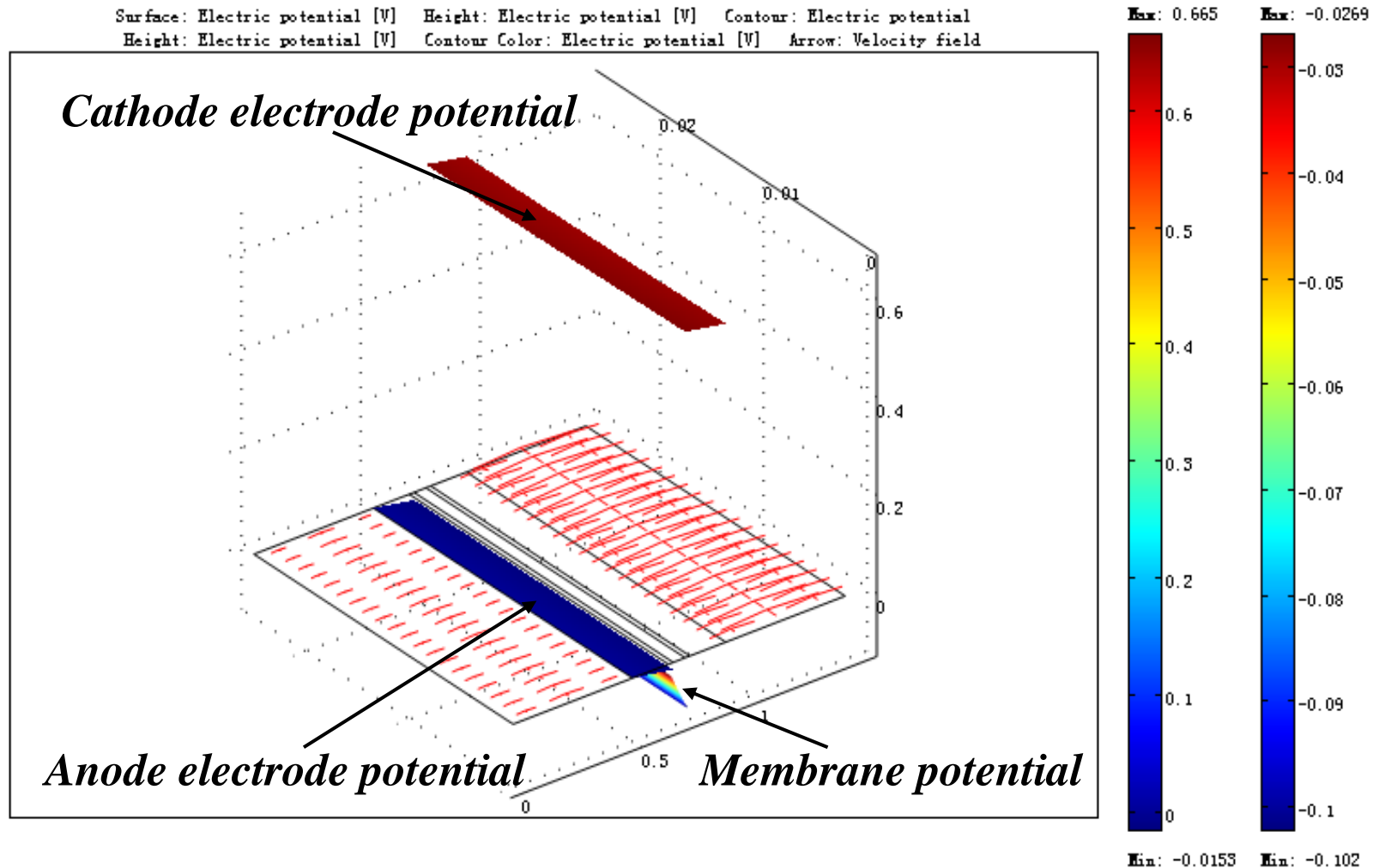
Species distribution in HT-PEMFC



Temperature distribution in HT-PEMFC



Potential distribution in electrode and membrane





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Conclusion

- ✓ Modeled fuel cell transient characteristics using COMSOL Multiphysics and the model result validated by experiment;
- ✓ Carried out fuel cell dynamic simulation using Comsol and closer to real operation conditions;
- ✓ Studied the effect of reactant transport and membrane water transport on the PEMFC cell potential under transient air flow and load change using COMSOL Multiphysics;
- ✓ Modeled the high temperature PEMFC based on Nafion/SiO₂ composite membrane using COMSOL Multiphysics .



Thank You !

