Study of Effect on Resonance Frequency of Piezoelectric Unimorph Cantilever for Energy Harvesting

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• 1



- Introduction
- Piezoelectric Effect
- Piezoelectric Cantilever
- Theoretical analysis using Matlab Simulink
- Modeling using COMSOL
- Conclusion
- References

Introduction

- At an average existing mobile Li Batteries has shelf life of 3-4 days.
- To investigate renewable power "scavenging" technologies.
- Piezoelectric materials can provide a direct transduction mechanism to convert signals from mechanical to electrical domains and vice versa.
- Piezoelectric materials are high energy density materials that are suitable for miniaturization. Therefore, this has led to a growing interest in piezoelectric thin films for MEMS applications.

Piezoelectric Effect

- Appearance of an electric potential across certain faces of a crystal when it is subjected to mechanical pressure
- The word originates from the greek word "piezein", which means "to press"
- Discovered in 1880 by Pierre Curie in quartz crystals.
- Conversely, when an electric field is applied to one of the faces of the crystal it undergoes mechanical distortion.
- Examples --- Quartz, Barium titanate, tourmaline



Electric dipoles in Weiss domains; (1) unpoled ferroelectric ceramic, (2) during and (3) after poling (piezoelectric ceramic)

Piezoelectric Effect





- displacement of electrical charge due to the deflection of the lattice in a naturally piezoelectric quartz crystal
- The larger circles represent silicon atoms, while the smaller ones represent oxygen.

Why Piezoelectric in MEMS

- Suitable for vibrational energy Harvesting
- Compatible with Microfabrication
- Voltages of 2-10V are obtained
- High energy density
- No separate external energy source needed
- Low maintenance
- Good efficiency

Piezoelectric Conversion



Piezoelectric Cantilever

Piezoelectric

Strain in piezoelectric material causes a charge separation



Design and Modeling Considerations

- Good quality material
- Low resistance
- Thermal management
- Higher power and frequency of operation

Theoretical Analysis

Piezoelectric Unimorph Cantilevers



Figure :The schematic of a PUC with the NPL/PL length ratio (a) >1, (b) =1and (c) <1, and the corresponding induced voltage distribution ((d), (e) and (f)) in the piezoelectric layer with a concentrated force, F, applied at the tip. Note that in (a)-(c), the dashed lines in Section-1 and Section-2 indicate the positions of the strain neutral plane.

Piezoelectric materials are characterized by several coefficients:



Resonant frequency (f_r)

$$f_r = \frac{\omega}{2\pi} = \frac{1}{2\pi} \sqrt{\frac{K}{m_e}}$$
(10)

Expressed in terms of Bending modulus per unit width Dp

$$f_{n} = \frac{v_{n}^{2}}{2\pi} \frac{1}{l^{2}} \sqrt{\frac{D_{p}}{m}}$$
(11)

$$m = \rho_p t_p + \rho_s t_s \tag{12}$$

$$D = \frac{E_p^2 t_p^4 + E_s^2 t_s^4 + 2E_p E_s t_p t_s (2t_p^2 + 2t_s^2 + 3t_p t_s)}{12(E_p t_p + E_s t_s)}$$
(13)

The induced voltage unit force $V_{in,ave/F}$ is given by

$$\frac{V_{in.ave}}{F} = \frac{1}{2} Lg_{31} \frac{E_p}{wD_1} \left(t_{n1}t_p + \frac{1}{2}t_p^2 \right)$$
(14)
$$K = \frac{2wD}{I^3}$$
(15)

The induced voltage per tip displacement $V_{in,ave/htip}$ is given by

$$\frac{V_{in.ave}}{h_{tip}} = \frac{3}{4} \frac{g_{31}E_s t_s E_p t_p (t_s + t_p)}{L^2 (E_s t_s + E_p t_p)}$$
(16)

Material properties of piezoelectric unimorph cantilever

Inputs to the model	ZnO	Pt		
Length(µm)	2500	2500		
Width(µm)	500	500		
thickness(µm)	2	4		
Young's modulus[GPa]	123-210	168		
Poisson's ratio		0.38		
Strain Coefficient(10 ⁻¹² m/v)	-5.4 - 11.67			
Density(Kg/m ³)	3980	21450		
Dielctric Constant(ε_r)	9-12.64			

Table :Material properties of piezoelectric unimorph cantilever

Simulink Model



Figure. Simulink model of piezoelectric unimorph cantilever

Simulation using COMSOL Multiphysics

Use of COMSOL Multiphysics

Application modes:

piezoelectric: Mechanical / Electrical behavior

- Generated charge / Electrical potential
- Vertical vibrations application

Moving Mesh: Varying Length



Geometry



Subdomain and Boundary settings

• Subdomain

ubdomains Groups	Damping	Initial Stress and	Strain	Init	Element Co	plor
ubdomain selection	Structural	Electrical	Constrai	nt	Load / Charge	
1	Structural settings					
<u>.</u>	Library material: Z	inc Oxide		•	Load	
	Material model:	Piezoelectric	•			
	Constitutive form:	Strain-charge form	n 👻			
	Coordinate system:	Global coordinate	system 👻			
	Quantity	Value/Expressio	n Unit De	scriptio	n	
	^s E	Edit	1/Pa Cor	npliance	matrix	
	d	Edit	C/N Cou	upling ma	trix	
Select by group	۴rT	Edit	Rel	ative per	mittivity	
	ρ	5680[kg/m^3]	kg/m ³ Der	nsity		
Active in this domain						

Subdomains Groups	Damping	Initial Stress and Strain		Init	Element Colo		
Subdomain selection	Structural	Electrical Constraint Loa			Load / Charge		
1	Load charge settings						
2	Coordinate system:	Global coordinate sy	ystem 👻				
	Quantity	Value/Expression	Unit	Descripti	on		
	Fx	0	N/m ³	Body load	(force/volume) X-dir.		
	FY	0	N/m ³	Body load	(force/volume) Y-dir.		
	Fz	a*rho_smpz3d	N/m ³	Body load	(force/volume) Z-dir.		
	Ρ _v	0	C/m ³	Space char	ge density		
-							
Group: 🚽							
Select by group							
Bolocc by group							
Active in this domain							

Zero charge

- Mechanical boundary conditions Floating potential

 fixed end
 Fixed

 Electric boundary conditions(piezo layer)
 - - Free end: grounded
 - fixed end: floating potential
 - other surfaces: zero charge

Ground

Governing equations

• Piezoelectric Equations in strain-charge form

 $S = s^{E}T + dE$ $D = \varepsilon^{T}E + dT$

S = mechanical strain T = mechanical stress [N/m²] s^E = elastic compliance [Pa⁻¹] d = piezoelectric coefficient [C/N] D = electric displacement [C/m²] E = electric field [V/m] $\varepsilon^T = dielectric permittivity [F/m]$

$\rho = 5680 Kg / m^3$

Meshing

Mapped mesh Parameter



Simulation Results

Eigen Frequency Analysis



Figure .Model frequency of piezoelectric unimorph cantilever.

Stationary Analysis



Figgure. Tip displacement due to applied Acceleration

Frequency Analysis





Figure : Frequency Response of d33

Time dependent Analysis



Harmonic vibration of 50 N/m2 amplitude with frequency from 450Hz to 510Hz is applied on the top surface of beam, so as to produce vibration. The resonant frequency for both d_{31} and d_{33} structure is 585 Hz

Force per unit area is taken as 50 *N/m*2 which is equivalent to a proof mass of 0.145 mg deposited on tip of cantilever at $9.81m/s^2$ acceleration.



Damping

Rayleigh damping for transient analysis

$$\begin{bmatrix} \frac{1}{2\omega_{1}} & \frac{\omega_{1}}{2} \\ \frac{1}{2\omega_{2}} & \frac{\omega_{2}}{2} \end{bmatrix} \begin{bmatrix} \alpha \\ \beta \end{bmatrix} = \begin{bmatrix} \zeta_{1} \\ \zeta_{2} \end{bmatrix} \qquad \zeta_{1} = \zeta_{2} = 0.1$$

$$\omega_{1} = 450$$

$$\omega_{2} = 510$$

Subdomains Groups Structural E

bdomain selection Damping Damping settings Library material: Material: Quantity Structural dampi adM BdK Coupling loss:	Initial Stress ar s : Zinc Oxide Piezoelectric, stra Value/Express ing: Rayleigh 49.5 1.98e-4	ain-charge	Init Load Description Mass damping	Element	Color
Damping settings Library material: Material: Quantity Structural dampi a _{dM} β _{dK} Counting locs:	s Zinc Oxide Piezoelectric, stra Value/Express ing: Rayleigh 49.5 1.98e-4	ain-charge	Load Description Mass damping	parameter	
Coupling loss		-	Stiffness dam	ping parameter	
up: Dielectric loss: Select by group Active in this domain	No loss No loss	•			

X

Output of Transient Analysis



Fig. . Frequency Response of *d*31 mode



Fig. . Frequency Response of d33 mode



Figure: Extrusion plot showing total displacement of d_{33}

Parametric Segregated Analysis Output



Figure: Plot of total displacement vs length in d31



Figure: Plot of total displacement vs length in d33



Figure : Extrusion plot for maximum voltage.



Min: 1.019e-12

Figure: Extrusion plot for maximum displacement.



• 33

Figure of Merit

Ref	Device	Dimension	V _{peak}	F(Hz)	Acceleration	V/mm ³	FOM
					g		V/mm ³ .g
[6]	<i>d</i> 31 PZT	2mm X 0.6mm X 1.64µm	0.45	608	1	228.7	228.7
[7]	<i>d</i> 31 PZT	2mmX3.2mmX1.39µm	16	60	0.79	112.4	142.3
[8]	<i>d</i> 31 ZnO	27mm x .3mm x 0.2mm.	4.7×10-9	10	0.1	2.9×10-4	.9×10 ⁻⁹
[9]	<i>d</i> 33 PZT	0.8mmX1mmX10 <i>µ</i> m	2.2	528	0.39	275	705
[10]	<i>d</i> 33 PZT	0.8mmX1.2mmX2 <i>µ</i> m	1.6	870	2	833.3	416.6
Proposed	<i>d</i> 31 ZnO	2.5mm x .5mm x 2μm.	1.05	485	1	420	420
Proposed	<i>d</i> 33 ZnO	2.5mm x .5mm x 2µm	4.2	485	1	1680	1680

Table . Performance Comparison reported MEMS Harvesters

Conclusion

- The work presents the study of piezoelectric cantilevers with engineered extensions to effectively convert ambient vibrations into electricity.
- Piezoelectric converters appear to be the most attractive for Microscale devices with a maximum demonstrated power density.
- Vibration powered systems are being actively pursued and will be up and running shortly.

Acknowledgement

- NPMASS(National program on micro and smart systems) of Govt of India and IISC Bangalore.
- Suyog N Jagtap for helpful suggestions in carry out this simulation work .

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Thank you.