

# Physical and FEM Simulation of Microprobe Insertion into Rat Brain

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**Abstract:** In order to investigate the implantation of microprobes into brain tissue, we developed a finite-element and a physical model to replace real biological tissue for mechanical testing. Penetrating forces of a tungsten indenter into a layered structure was investigated with different indentation speeds. Numerical and physical model are in good correspondence to each other and reproduce measured brain elasticity (15kPa) and dimpling effects followed by rupturing of the top layer well. We suggest for future mechanical evaluation of brain probes to first utilize model structures before sacrificing animals.

**Keywords:** microprobes, indentation, dimpling.

## 1. Introduction

One of the most exciting developments during the last few years connecting basic research with almost immediately useful clinical technology was the successful application of multiwire neuronal recordings with advanced signal processing to utilize intracortical neuronal signals to control devices [2-6]. Unfortunately penetrating rigid microelectrode arrays traumatize surrounding tissue in such a way, as to render the recording sites over time useless due to severe foreign-body reaction [7-12].

The first development of flexible microprobes [13] carrying microelectrodes (for recording and stimulation) in parallel with appropriate chemical surface coating [14] or even living cells [15, 16] holds the promise for an optimized integration into brain tissue.

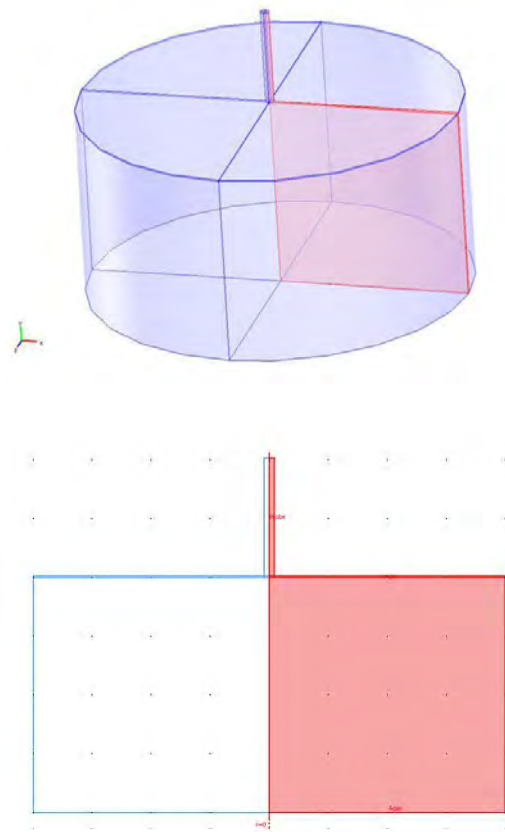
Still, not too much attention has been given to the implantation procedure itself, besides the development of the pneumatic inserter for bed-of-nail type silicon arrays [17]. On the other hand, slow and gentler implantation of microprobes is known to cause a severe dimpling effect and as such may damage superficial neuropil even before the immune response starts. In the following, we want to introduce a physical and computational small scale model of the brain surface as it is usually exposed by a craniotomy in laboratory animals. The purpose of our models

is to test and improve the mechanical properties of new multisite microprobes during insertion without the need for animals.

## 2. Materials and Methods

### 2.1 Computational finite-element model

An axisymmetric indentation model of a layered structure was developed using COMSOL 3.5a (Comsol Multiphysics GmbH, Göttingen). The model had three components (see Fig. 1) - a flat tip cylindrical probe (the „microprobe“), one thin elastic layer (the „pia mater membrane“) and viscoelastic bulk material under it.



**Figure 1:** (top) 3D model of an indenter-membrane-bulk structure, (bottom) 2D view and half slice of the same model.

The „microprobe“ was simulated as a flat ended cylinder with 90 $\mu$ m diameter and 1mm in length. Its material properties were set to match Tungsten with a Young’s modulus  $E=3.6 \times 10^{11}$ Pa and Poisson’s ratio  $\nu=0.27$ .

The „pial membrane“ was designed to match an elastic material formed of PE-polymer ( $E=2.9 \times 10^9$ ) and  $\nu=0.33$  [18].

The bulk material is modeled by a generalized Maxwell model [19] with the associated model parameters of 1% (w/v) agar-gel shown in Table 1.

| $G$ (kPa) | $G_i$ (kPa) | $\tau_i$ (s) |
|-----------|-------------|--------------|
| 4.667     | 1.416       | 14.41        |
|           | 4.977       | 159.62       |

**Table 1:** viscoelastic parameters of Agar material

Foil-layer which is located between the probe and the Agar has a 15 $\mu$ m of thickness and 4mm of diameter, the Agar which is the biggest object modeled as cylinder of 4mm of diameter and 2mm of height.

The microprobe was loaded with a prescribed displacement in z-direction with  $R_z = v \cdot t$  ( $R_z$ : the displacement,  $v$ : velocity of the probe motion,  $t$ : elapsed-time of the probe motion). The probe was fixed in the r-direction at  $R_r = 0$ ; the left hand side boundary of all three parts complies to a symmetry plane condition; the right hand side of the membrane-layer is fixed, the right hand side and bottom of the bulk are fixed too, all other boundaries are left free.

We solved our model as an axisymmetric problem with the COMSOL provided method as a transient analysis. The necessary elapsed time parameter was deduced from the experimental indentation data.

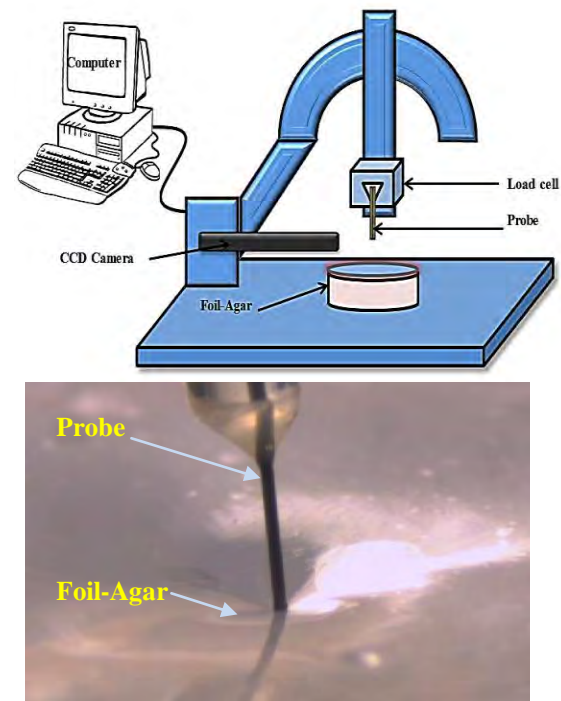
## 2.2. Physical indentation model

A 1% (w/v) agar gel was prepared by dissolving microbiological grade granulated agar (Agarose NEE0, Carl Roth GmbH, Karlsruhe, Germany)) in distilled water. The solution was heated to boiling in an Erlenmeyer flask on a hot plate. The liquid agar dispersion was poured into a 37mm petridish and cooled overnight at room temperature for testing 24 h later ( $\pm 2$  h). Commercial food wrapping foil with 15 $\mu$ m

thickness (Poylethylen, Aromata, Lidl) was tightened without air traps on top of the agar gel and fixed on the petridishes rim.

A 1mm long and 90 $\mu$ m diameter tungsten rod with a flat end was fixed by a Luer-connector in a high precision commercial 5DOF stereotactic frame (SASSU, pro-medTEC GmbH, Lübeck) [20] equipped with a force measuring load cell ( $\pm 300$ mN, SS2 Sherborne Sensors, Hampshire, UK).

The frame reached a maximum insertion speed of up to 3mm/s. We determined by video analysis (see Fig. 2) the actual time spans from first contact of the probe with the foil/agar model to the rupturing of the foil for six different indentation speeds (0.25, 1, 2, and 3mm/s).



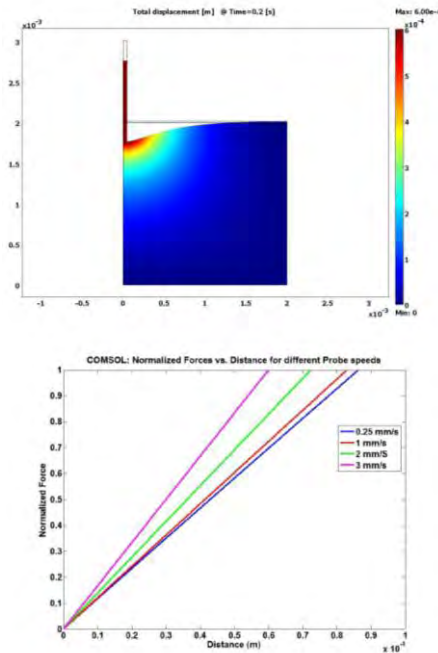
**Figure 2:** (top) Sketch of experimental setup to measure probe indentation into brain model; (bottom) single video frame from 0.25mm/s indentation of a 90 $\mu$ m tungsten rod into PE foil/1%agar substrate.

Load cell readouts during penetration are recorded as output voltage per time (data logger DI-718b USB, Dataq Instruments, Akron,OH). These values are then converted to forces with help of the documented the load cell sensitivity and the known SASSU parameters.

### 3. Results

#### 3.1. FEM results

The simulation of the two-layer structure displayed the experimentally recognizable deformation and thus effects of dimpling, but was limited to an unruptured top layer.

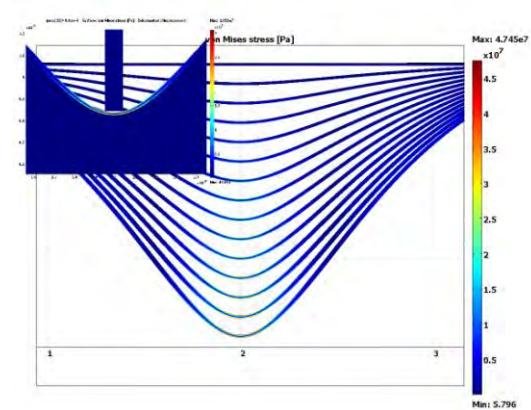


**Figure 3:** (top) Simulation of indenting a blunt tip into our layered model with 5mm/s speed; (bottom) Normalized force-distance plot for six different indentation speeds (0.25, 1, 2, and 3mm/s).

Consequently, we only display the spatial deformation of the indentation, caused by a displacement of the bulk agar under the top membrane (see Fig. 3 top). Displaying force vs. distance curves showed a quite characteristic linear increase in forces, until the van Mises stresses in the pial simulation exceeded the critical value, where the force relaxes in the experiment by breaking through the membrane (Fig. 5). To keep results comparable (absolute data not shown), we normalized the force-distance curves to the maximum force prior to pial rupture. When comparing the slopes of these

curves, a clear dependency on the simulated penetration speed can be seen (Fig. 3 bottom). Closer investigation of the possible location of rupture in the pial membrane during increasing loads shows excessive peaking of van Mises stress at the edges of the indenter (Fig. 4).

#### 3.2. Foil/Agar indentation



**Figure 4:** (insert) Simulation of a blunt indenter into a layered model; (graph) Overlay of consecutive time steps of indentation, indicating an increasing van Mises stress at the probes front edge.

Indentation of a tungsten rod into the foil/agar layer showed qualitatively a dimpling effect comparable to that of a microprobe through a rat's pia. However, when the penetration force with the former reached 30mN, forces with the latter stayed below 10mN (for a 50µm tungsten rod) [21].

When force-distance curves on foil/agar are displayed, they show an almost linear increase in force after first contact, which corresponds nicely to the simulated curve shapes. Even the speed dependency of the curves are maintained, when normalizing the measured forces to the maximum (penetration) force (see Fig. 5).

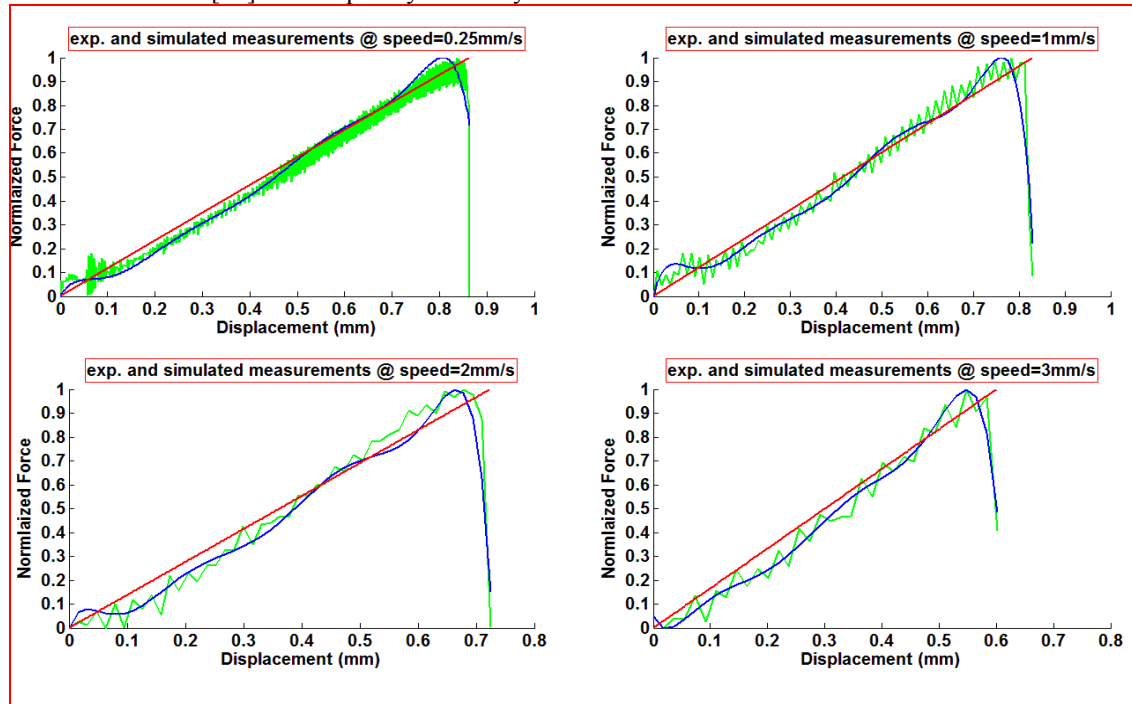
The elastic modulus of 1% Agar was calculated with the following shear modulus formula

$$E = 2 G (1 + \nu)$$

with  $G$  being the shear modulus ( $4.667 \times 10^3$  Pa),  $\nu$  the Poisson's ratio and  $E$  the elastic modulus [22].

Since the agar material is considered a viscoelastic material its Poisson's ratio was assumed to be 0.5 [23]. Consequently elasticity

of 1% Agar gel lies around 15kPa, which compares reasonably with results from living rat brain (6 - 20kPa) [25].



**Figure 5:** Force-distance curves for several indentation speeds. (green): experimental data, (blue): polynomial fit of experimental data and (red): FEM simulation result.

#### 4. Discussion

Main motivation for this study was to provide the methodological means to evaluate new probe designs and implantation methods by reasonable models without the need to sacrifice animals. Even though the physical simulated elasticity of 1% agar falls in the same range as cortical rat brain does, agar itself is not suitable to solely model the real tissue. This is mainly due to the lack of a tough surface membrane on agar, as can be found in the hard to remove pia mater of the animal's brain.

Consequently some surface layer has to be introduced, which at least somewhat resembles the elastic properties of the pial membrane. With the use of PE-food wrapping foil on top of agar, we are able to reproduce the recorded dimpling of the penetrated tissue and such are closer to the real situation. Still, even this model has its

shortcomings, mainly since the PE foil does not completely copy the pia, which makes it seemingly harder to penetrate and thus needs higher implantation forces, not to be reached by silicon probes!

However, a FEM simulation may very well be able to provide desired model. Our two layer indenter model at least provided results for different indentation speeds we tried, which very well match the implantation behaviour, except (due to numerical reasons) the rupturing itself.

At least the FEM simulation gave by hints as to where the rupturing will occur, according to its van Mises stress distribution. This approach will in the future enable us optimize micromachined probe shapes to enable elegant implantation without forced insertion. Up til then we do suggest the use of high speeds for implantation through the pia over slow and careful implantation.

## 5. Acknowledgements

Part of this work was supported by the BMBF-grant 13N9190 "BiCIRTS".

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