



ALTASIM
TECHNOLOGIES
REALIZING TOMORROW'S TECHNOLOGY

Multiphysics Analysis of Thermoelectric Phenomena

S.P. Yushanov, L.T. Gritter, J.S. Crompton and K.C. Koppenhoefer

AltaSim Technologies, LLC

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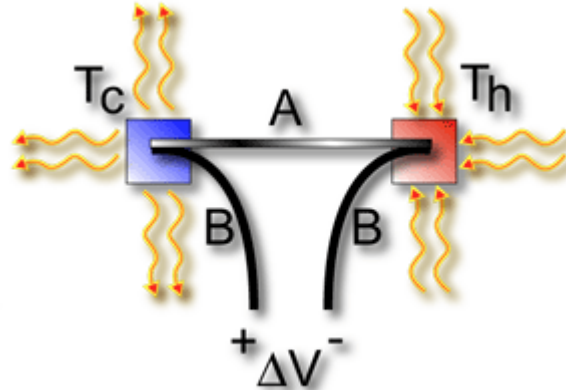


Thermoelectric materials

- **Behavior described by effects:**
 - Seebeck
 - Peltier
 - Thomson
- **Effects linked:**
 - Seebeck is result of Peltier and Thomson

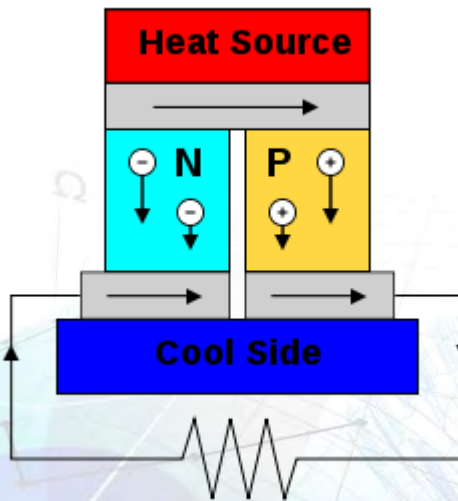
Thermoelectric materials

- **Seebeck effect:**
 - Voltage due to temperature difference
 - Example: Thermocouples, energy conversion



Thermoelectric materials

- **Peltier effect:**
 - Temperature at junction of two materials due to flow of current
 - Direction of current flow determines heating/cooling
 - Examples: Solid state heating/cooling

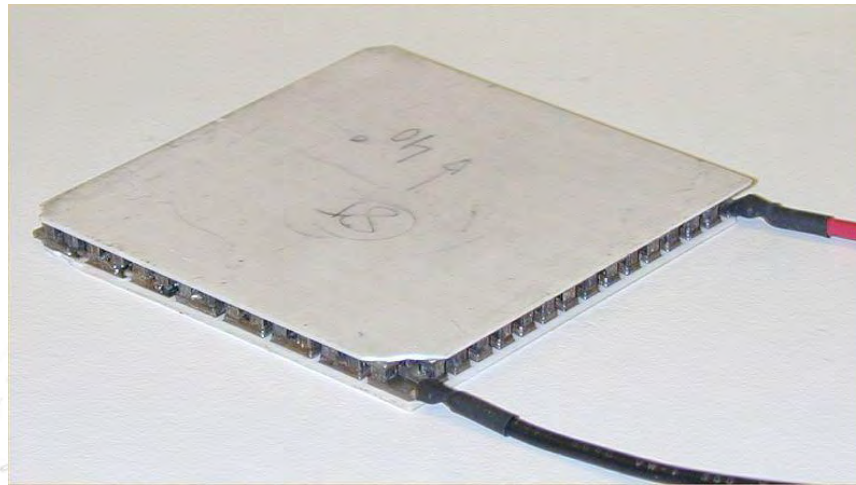


Thermoelectric materials

- **Thomson effect:**
 - **Current flow in a temperature gradient**
 - **Power absorbed or rejected**
 - **Heat is proportional to electric current and temperature**
 - **Seebeck is result of Peltier and Thomson effects**
 - Thomson's second relationship: $P = -S \cdot T(K)$

Thermoelectric devices

- Arrays of Peltier cells
- Typically Bismuth Telluride
- Doped “n” or “p” type semiconductors
- Solid state heaters/coolers, thermocouples



Governing equations

- **Electric current balance:** $-\nabla \cdot (\sigma \cdot \nabla V) = 0$
- **Heat energy balance:**
$$\begin{cases} \rho C_p \frac{\partial T}{\partial t} + \nabla \cdot \mathbf{q} = Q \\ \mathbf{q} = -k \nabla T + \underline{\underline{PJ}} \end{cases}$$
- **Thomson's second relationship:** $P = -ST$
- $Q_{\text{tot}} = Q_{\text{heat pump}} + Q_{\text{resistive}} + Q_{\text{conductive}}$

Implementation in COMSOL

- FE methodology
- Weak form implementation
 - Implement in heat transfer module
 - Convert energy balance to weak form
 - Multiply each side of energy balance equation by test function
 - Integrate over the computational domain

$$\int_{\Omega} \rho C_p \frac{\partial T}{\partial t} T_{test} d\Omega + \int_{\Omega} (\nabla) T_{test} d\Omega = \int_{\Omega} Q T_{test} d\Omega$$

Weak form implementation

- Apply vector identity:

$$\nabla \cdot (T_{test} \mathbf{q}) = \mathbf{q} \cdot \nabla T_{test} + T_{test} \nabla \cdot \mathbf{q}$$

- Equation becomes:

$$\int_{\Omega} \rho C_p \frac{\partial T}{\partial t} T_{test} d\Omega + \int_{\Omega} \nabla \cdot (T_{test} \mathbf{q}) d\Omega - \int_{\Omega} \mathbf{q} \cdot \nabla T_{test} d\Omega = \int_{\Omega} QT_{test} d\Omega$$

Weak form implementation

- Apply Gauss' theorem:

$$\int_{\Omega} \nabla(T_{test} \cdot \mathbf{q}) = \int_{\partial\Omega} T_{test} \mathbf{q} \cdot \mathbf{n} \partial\Omega$$

- Revised equation:

$$0 = \int_{\Omega} \left[-\rho C_p \frac{\partial T}{\partial t} T_{test} + \mathbf{q} \cdot \nabla T_{test} + QT_{test} \right] d\Omega - \int_{\partial\Omega} (\mathbf{q} \cdot \mathbf{n}) T_{test} \partial\Omega$$

Weak form implementation

- Energy flux:

$$\mathbf{q} = -k\nabla T + P\mathbf{J}$$

- Revised equation:

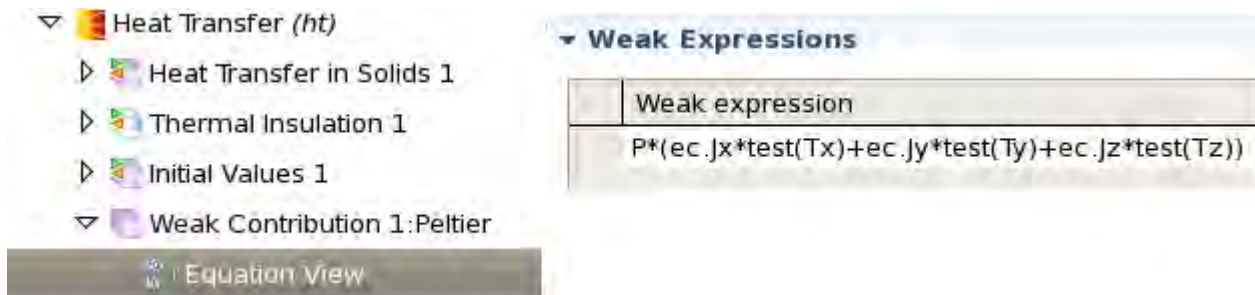
$$0 = \int_{\Omega} \left[\underbrace{-\rho C_p \frac{\partial T}{\partial t} T_{test}}_{dweak} + \underbrace{(-k\nabla T) \cdot \nabla T_{test}}_{weak\ thermal} + \underbrace{(P\mathbf{J}) \cdot \nabla T_{test}}_{weak\ Peltier} + \underbrace{QT_{test}}_{weak\ source} \right] d\Omega - \int_{\partial\Omega} \underbrace{(\mathbf{q} \cdot \mathbf{n}) T_{test}}_{Neumann\ BC} d\Omega$$

- Weak Peltier contribution:

$$\begin{aligned} weak_p &= (P\mathbf{J}) \cdot \nabla T_{test} = PJ_x \frac{\partial T_{test}}{\partial x} + PJ_y \frac{\partial T_{test}}{\partial y} + PJ_z \frac{\partial T_{test}}{\partial z} = \\ &= P * ec.Jx * test(Tx) + P * ec.Jy * test(Ty) + P * ec.Jz * test(Tz) \end{aligned}$$

Weak form implementation

- Implement weak Peltier contribution in Heat Transfer module:



The screenshot displays a software interface for defining weak expressions. On the left, a tree view shows the hierarchy: Heat Transfer (ht) > Heat Transfer in Solids 1 > Thermal Insulation 1 > Initial Values 1 > Weak Contribution 1:Peltier. The 'Equation View' button is highlighted at the bottom. On the right, the 'Weak Expressions' table is shown with the following content:

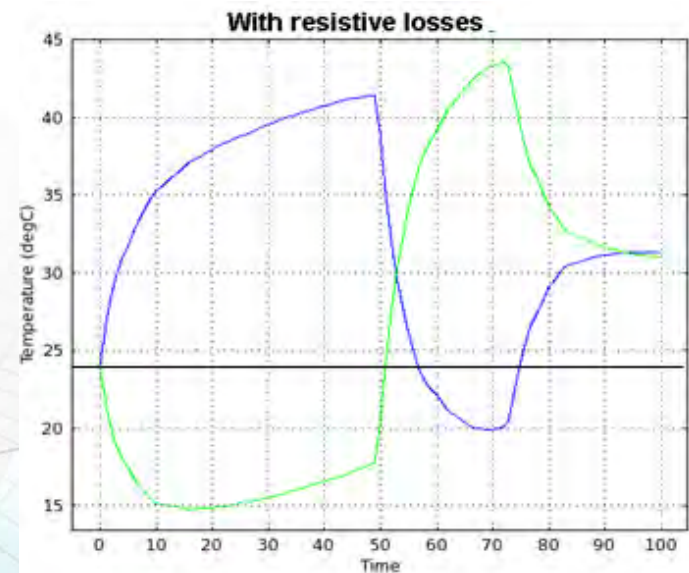
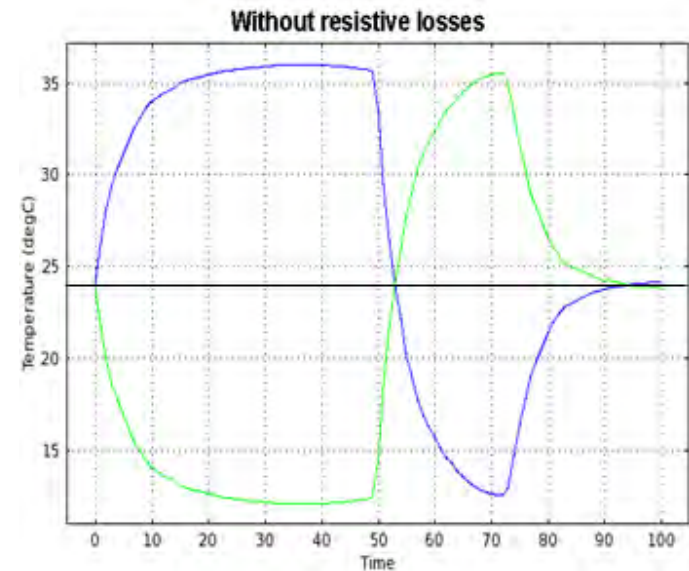
Weak expression
$P*(e_c.j_x*test(T_x)+e_c.j_y*test(T_y)+e_c.j_z*test(T_z))$

COMSOL Multiphysics analysis

- **Peltier contribution**
 - Weak form
- **Temperature dependent material properties**
 - Peltier/Seebeck coefficients
 - Thermal conductivity
 - Electrical conductivity

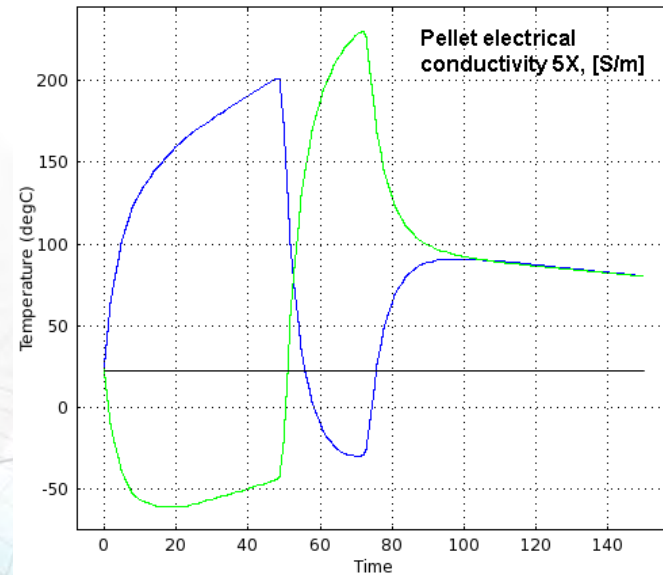
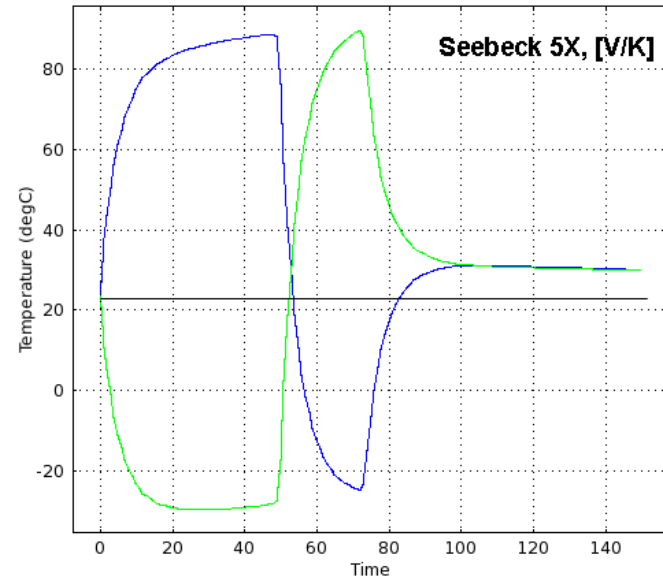
Property variations

- Effect of resistive losses
- TEM
 - Applied current vs time history
 - Effect on hot and cold sides



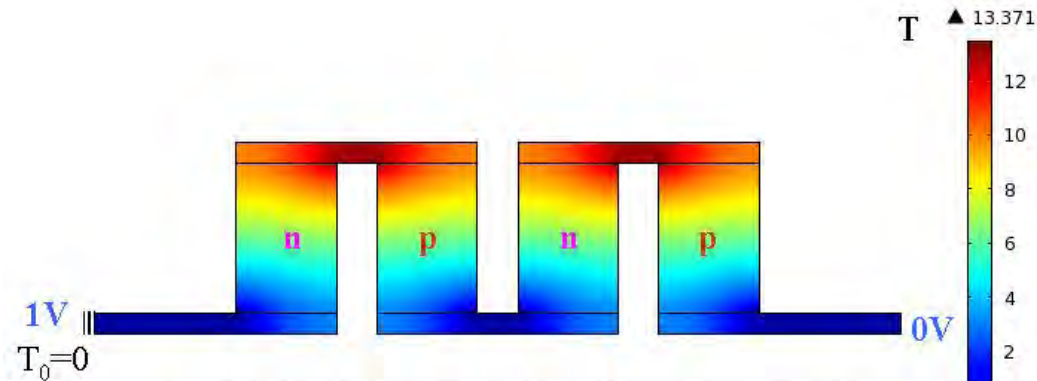
Property variations

- TEM: Applied current vs time history
- Effect of variation in Seebeck coefficient of 5x
- Effect of variation in electrical conductivity of 5x

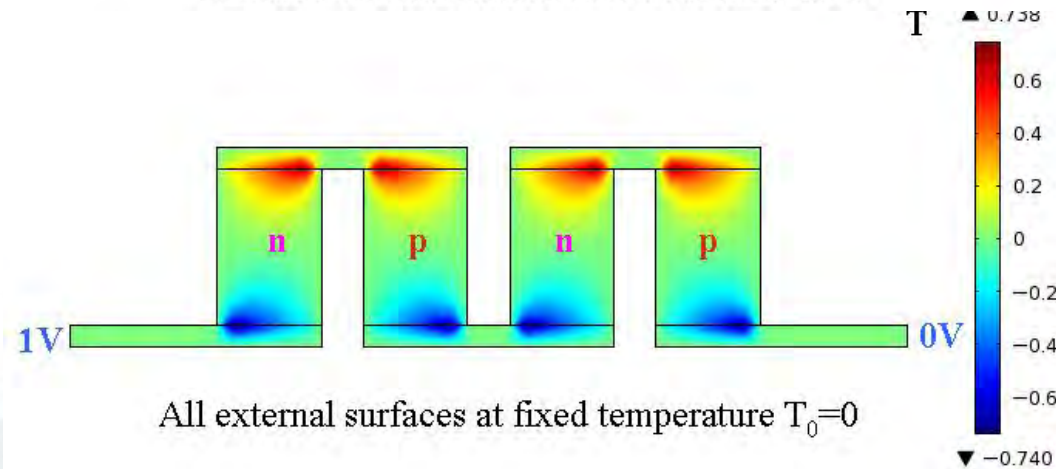


Analytical results: Peltier

- BiTe₃ p-n junctions subject to imposed voltage
- Temperature distribution developed
- Solid state heater/cooler



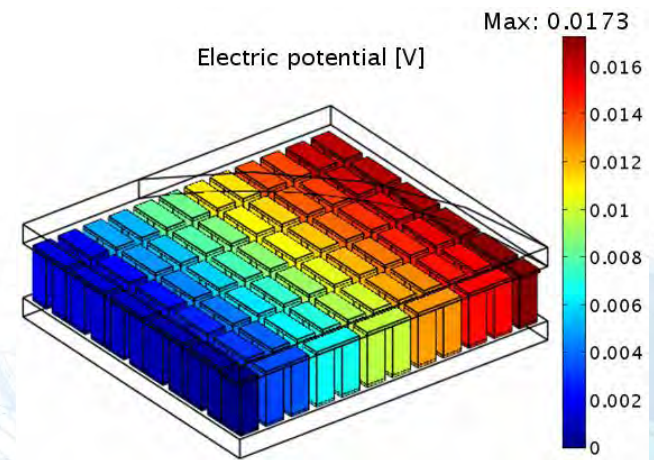
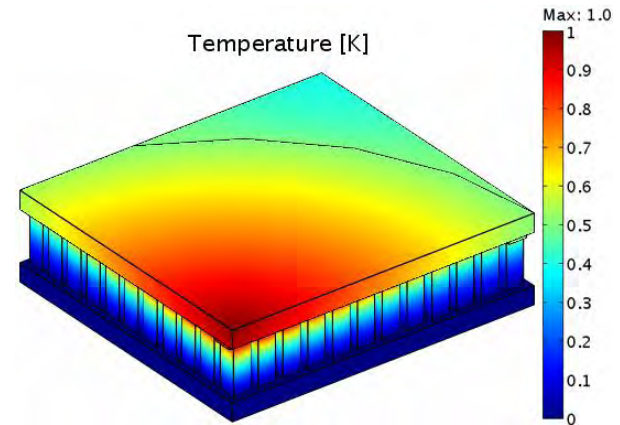
Left side of electrode at fixed temperature $T_0=0$
All other external surfaces are thermoinsulated



All external surfaces at fixed temperature $T_0=0$

Analytical results: Seebeck

- Imposed thermal gradient in BiTe₃ TEM
- Current generated in array of cells
- Magnitude of generated current depends on temperature difference



Summary

- **Peltier/Seebeck terms implemented using weak form methods**
- **Fully coupled temperature dependent material properties**
- **Predict effect of imposed thermal gradients**
- **Predict effect of electric current flow**